

# INDIANA DEPARTMENT OF HIGHWAYS

JOINT HIGHWAY RESEARCH PROJECT JHRP-85-15

ENGINEERING SOILS MAP OF HUNTINGTON COUNTY, INDIANA

Edward M. Gefell





PURDUE UNIVERSITY



# Final Report

# ENGINEERING SOILS MAP OF HUNTINGTON COUNTY, INDIANA

TO: H. L. Michael, Director

Joint Highway Research Project

August 28, 1985

Project: C-36-51B

FROM: Robert D. Miles, Research Engineer

Joint Highway Research Project

File: 1-5-2-76

The attached final report entitled "Engineering Soils Map of Huntington County, Indiana" completes a portion of the longterm project concerned with the development of a county engineering soils map of the 92 counties of the State of Indiana. This is the 76th report of the series. The report was prepared by Edward M. Gefell, Research Associate, Joint Highway Research Project.

Mr. Gefell developed the engineering soils map using aerial photographs, available literature, available soil borings, and limited field studies. Generalized soil profiles of the major soils of each land form-parent material area are presented on the engineering soils map included. The map and report should be useful in planning and developing engineered facilities in Huntington County.

Sincerely,

Robert Miles

Robert D. Miles, P.E. Research Engineer

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Ъу

Edward M. Gefell Research Associate

Joint Highway Research Project

Project No.: C-36-51B

File No.: 1-5-2-76

Prepared as Part of an Investigation

Conducted by

Joint Highway Research Project Engineering Experiment Station Purdue University

in cooperation with

Indiana Department of Highways

Purdue University West Lafayette, Indiana

August 28, 1985



## ACKNOWLEDGMENTS

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Professor Harold L. Michael, Director, Joint Highway Research

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Special thanks goes to Professor Robert D. Miles for his

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# ENGINEERING SOILS MAP OF HUNTINGTON COUNTY, INDIANA

## INTRODUCTION

The Engineering Soils Map of Huntington County, Indiana (see developed primarily by interpretation of 1937 Figure 1) was aerial photographs using accepted principles of observation and deductive reasoning (1)\*. A photomosaic of the county was assembled and land form - parent material associations were delineated by stereoscopic inspection. Available literature, particularly the Soil Conservation Service (SCS) publication "Soil Survey of Huntington County" (2), and topographic, drainage, bedrock and glacial maps as well as roadway soil survey borehole data were referred to while making soil boundary adjustments on the photomosaic. The scale of the aerial photographs used in this project, which were purchased from the United States Department of Agriculture, was approximately 1:20,000. A photomosaic of Huntington County is shown in Figure 2.

A one-day field trip was taken to the county to check soil boundaries, correlate surface soil textures with airphoto patterns observed in the laboratory and resolve ambiguous details. Soil boundaries were modified as necessary according to observations made and soil samples examined in the field. The soil samples taken extended to a depth of approximately 3.5 feet and were used to determine the nature of the surface and subsoils

<sup>\*</sup> Note: Numbers in parenthesis footnote references.



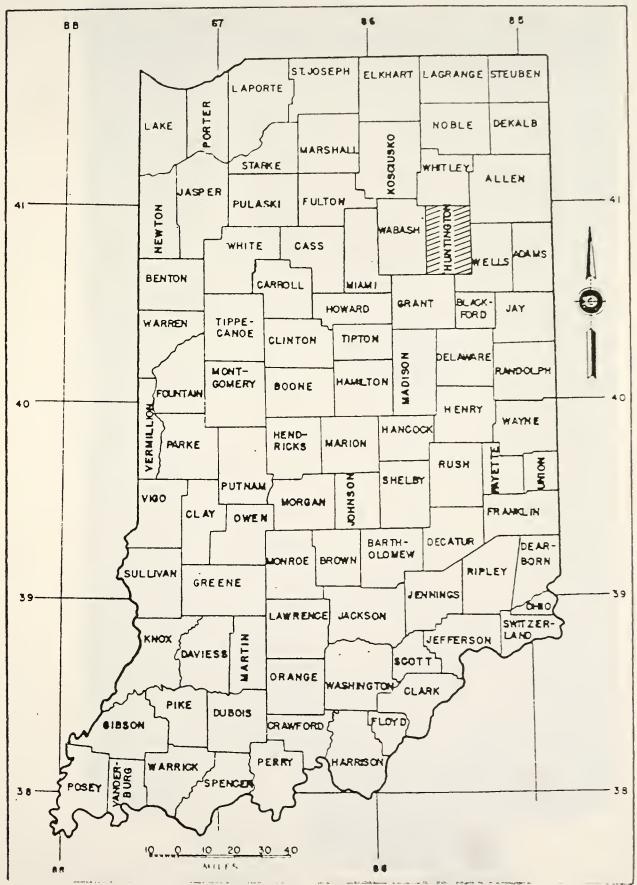


Figure | Map of Indiana Showing Location of Huntington County



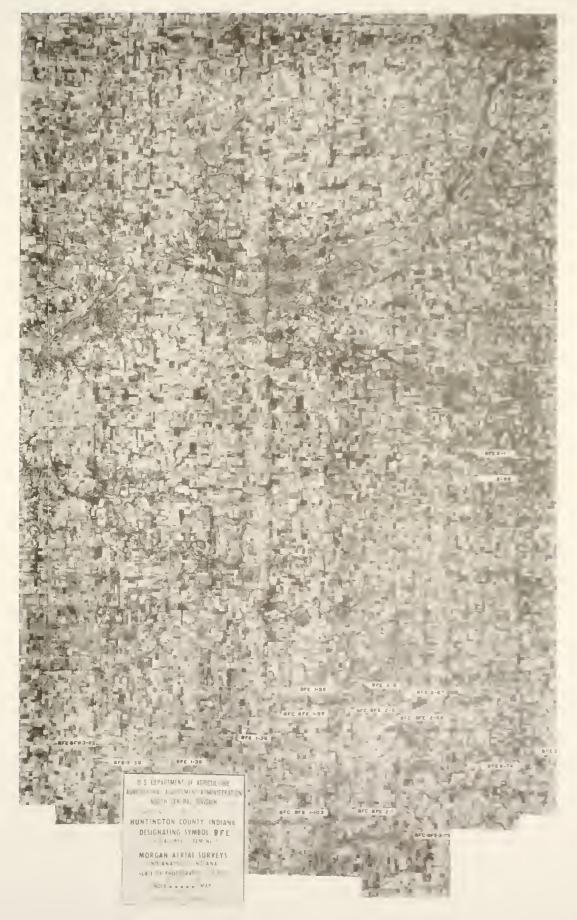


Figure 2. 1938 Photomosaic of Huntington County, Indiana



developed over the various parent materials in Huntington County.

The information obtained from the hand-sampling was used with roadway and agricultural soil survey data in the development of general land form - parent material association soil profiles shown on the left-hand side of the engineering soils map.

The Engineering Soils Map of Huntington County, Indiana represents part of a comprehensive, county by county, engineering soil survey of the State of Indiana using a standard set of symbols developed by the Airphoto Interpretation Laboratory, School of Civil Engineering, Purdue University. A primary objective of mapping project was to develop a survey whereby all soil the boundaries and land form - parent material associations correlated across county lines. In the process of airphoto interpretation, some subjective disagreement may occur as to the nature of given soil unit and the location of its boundaries. Where the interpretations of this author differed from those of authors of adjacent counties, every effort was made to determine the land form pattern percieved by the other author and integrate the given soil unit into the soil boundary pattern of Huntington County. In some instances, soil boundaries were terminated rather abruptly, very near to the Huntington County line. Some of the anomalous areas were controversial due to a lack of adequate relief (ie., less than five feet) on which to base a judgement for boundary placement by stereoscopic inspection. Other disputed areas resulted from differences in mapping detail between Huntington and adjacent counties.



The text of this report supplements the engineering soils map and includes a general description of the study area as well as more detailed information about the various land form - parent material associations found in Huntington County. The map itself shows the land form - parent material areas, surface soil textures and generalized soil profiles. Available roadway soil survey data for the numbered boreholes shown on the map and the engineering properties, characteristics, and suitability of the pedalogical soil series mentioned with regard to the various land form - parent material associations are given in appendices in the back of this report. Information contained in the appendices includes the following:

- 1. Appendix A-1, Estimated Engineering Properties
- 2. Appendix A-2, Physical and Chemical Soil Properties
- 3. Appendix A-3, Soil and Water Features
- 4. Appendix A-4, Construction Materials
- 5. Appendix A-5, Building Site Development
- 6. Appendix A-6, Sanitary Facilities
- 7. Appendix A-7, Water Management
- 8. Appendix A-8, Recreational Development

  All of the material in Appendix A was taken directly from the SCS

  Soil Survey of Huntington County (2).



# DESCRIPTION OF THE AREA

## General

Huntington County is located in the northeast part of the State of Indiana and has an approximate area of 390 square miles, or 249,600 acres (2). Huntington County is bordered to the north by Whitley County, to the east by Allen and Wells Counties, to the south by Wells and Grant Counties and to the west by Wabash County. The City of Huntington, located in the north-central part of the county near the junction of the Wabash and Little Wabash Rivers, approximately 85 miles northeast of Indianapolis, is the seat of county government.

Huntington County had a total population of 35,596 in 1980 of which 20,687 lived in cities and towns, while 14,909 lived in rural areas (3). Table 1 lists the population of the major cities and towns in Huntington County.

Table 1. 1980 Population of Cities and Towns in Huntington County, Indiana (3).

City/Town	Population
Andrews Huntington Markle + (Wells Co.) Mt. Etna Roanoke	1,243 16,202 975 122 891
Warren	1,254

Population increased by less than 1,000 over the 1970 figure for



Huntington County.

Huntington County is served by State, Federal, and Interstate highways. Interstate 69 cuts across the southeast part of the county, turning northward near Markle before crossing the Wells County line east of the City of Huntington. U.S. Highway 24 extends northeastward to Fort Wayne and westward to Wabash from the City of Huntington. U.S. 224 extends southeast from the city into Wells County. State highways include S.R. 3, 9, 105 and 221 in the north-south direction and S.R. 16, 24, 114 and 218 in the east-west direction. S.R. 37 extends diagonally across the county (via S.R. 9 and U.S. 24) from the southwest to the northeast corner of the county while S.R. 5 passes through the City of Huntington in a northwest-southeast direction.

Railroads provide freight service from the City of Huntington to Chicago and Fort Wayne and to neighboring Wabash and Wells counties and points beyond (2). The city has no rail passenger transportation. The Huntington County municipal airport is located about two miles southeast of the city and provides for limited commuter and private flights.

Approximately 159,059 acres were in cropland in Huntington County in 1974, down 6.3 percent from 1969 (2). Urban land continued to increase at the expense of cropland, particularly around the city of Huntington and toward the northeast part of the county along the U.S. 24 corridor to Fort Wayne. Roughly seven percent of the county was in woodland in 1974.



Ground water provides the primary source of potable water in Huntington County (2). Drinking water is supplied by eight deep wells for the City of Huntington and is supplemented by water from the Wabash River for some industrial and municipal purposes. The flood control Huntington Reservoir, located on the Wabash River about three miles southeast of the county seat, and the Salamonie Reservoir, which crosses the Wabash County line in the Salamonie River Valley, serves as recreational areas for the county populace.

# Climate

Huntington County is located in a region of temperate climate in the North American mid-continent. The area experiences invigorating weather with occasional extreme fluctuations in temperature on a daily basis and a wide range of temperatures seasonally. Weather fronts, associated with passing pressure systems, bring rapid temperature changes and the potential for severe weather including high winds, heavy snowfall, thunderstorms, hail, and heavy rainfall, depending on the time of year. Atmospheric changes are most dramatic during the spring and least so during late summer and early fall.

Temperature extremes included a record high of  $110^{\circ}$  F in July, 1936 and a record low of  $-20^{\circ}$  F in January,  $1936^{*}$  (4). The highest mean daily maximum temperature of  $86.8^{\circ}$  F occurred in July, the hottest month of the year, while the lowest mean daily

<sup>\*</sup> Note: records refer to the period 1934-1963.



minimum of  $18.2^{\circ}$  F occurred during the month of January. January had a monthly mean temperature of  $26.3^{\circ}$  F and July experienced a monthly mean temperature of  $74.2^{\circ}$  F. The thermometer registered  $90^{\circ}$  F or higher an average of 27 days and remained below freezing about 38 days per year. The temperature dropped below  $0^{\circ}$  F about seven times per year.

Precipitation is distributed fairly evenly throughout the year, with the spring and early summer receiving somewhat more than the rest of the year. A high monthly mean of 4.21 inches fell in June while a monthly minimum of 2.06 inches fell in December. A record 5.07 inches of rain fell on a June day in 1959. An average of 25 inches of snow fell per year, most of it coming during the period December through March (5). Total yearly precipitation amounts to about 22 inches.

Severe weather, commonly associated with frontal systems, includes thunderstorms which occur primarily between the months of April and October, and a rare tornado which is most likely to occur in the spring of the year when the atmosphere is most active.

Climatic data for Huntington County is summarized in Table 2.



LATITUDE 40° 53' N. LONGITUDE 85° 30° W. FIEV (GROUND) 802 Ft.

# Table 2. Climatological Summary (4) STATION HUNTLINGTON, INDIANA

MARKE AND EXTREMES BOR RESIDE 1934-1963

			Tem	peratu	re (°F)			:		P	recipital	tion To	otals (L	nches)			Me	an na	ımbe	r of d	Aya	
		Means			Extre	emes		days					8n	ow, 51	•• t		acb			rabize		
		1.100111						8		daily					,		-	M	AZ.	М	in.	
Month	Daily maximum	Daily minimum	Monthly	Record highest	Year	Record lowest	Year	Mean degree	Mean	Greatest da	Year	Meen	Maximum monthly	Year	Greatest daily	Year	Precip10 or more	90° and	32° and below	32° and below	O' and below	Month
(a)	30	30		30		30		30	30	30		30	30		30		10	30	30	30	30	
Jan.	34.4	18.2	26.3	65	1952	-20	1936	1150	2.64	2.16	1950	6.5	18.0	1939	6.0	1950	5	0	13	29	3	Jøn.
Feb.	37.5	20.2	28.9	70	1954	-18	1951	997	2.29	2.52	1936	7.3	15.3	1960	8.0	1952	5	0	9	26	2	Fab.
Mar.	47.9	28.2	38.1	84	1938	-8	1948	853	3.36	2.20	1945	3.9	11.0	1947	5.0	1955	8	0	3	22		Mar.
Apr.	61.2	38.3	49.8	89	1942	14	1940	456	3.67	1.85	1944	1.6 T	15.2	1961	6.9	1961	7	0		9	0	Apr.
May	72.9		60.6	95	1934	24	1947	195 39	4.06	2.81	1946	_	T	1960+	T	1960⊲	8	1	0	1	0	May
June	82.7	57.9	70,3	106	1934	35	1945	39	4.21	5.07	1959	0	0		٥		8	6	0	0	0	Juns
July	86.8	61.6	74.2	110	1936	42	1941	0	3.57	3.65	1942	0	0		0		8	9	0	0	0	July
	85.5	60.2	72.9	105	1934	35	1946	0	2.96	3.15	1943	0	0		ō		5	7	0	0	0	Aug.
Sept.		52.2	65.4	103	1953+	26	1951	90	2.66	2.47	1950	0	0		0		6	4	0	1	0	Sept
Oct.	67.4	42.3	54.9	91	1953+	16	1952	338	2.87	2.93	1955	Ţ	0.6	1962	0.6	1962	5	•	0	5	0	Oct.
Nov.	49.7	31.7	40.7	81	1950	-5	1950	732	2.67	2.99	1936	2.8	12.5	1950	7.0	1950	6	0	2	17	•	Nov.
Dec.	36.8	21.4	29.1	68	1951	-15	1951	1082	2.06	1.64	1936	6.4	16.0	1950	5.1	1960	5	0	11	26	2	Dec.
Year	61.8	40.0	50.9	110	July 1936	-20	Jan. 1936	5932	37.02	5.07	June 1959	28.5	18.0	Jøn. 1939	8.0	Fwb. 1952	76	27	38	135	7	Year

- (a) Average length of record, years.
- I Trace, an amount too small to measure.
- 40 Rose 650P

- + Also on earlier dates, months, or years.
- \* Less than one half.

CLIMATE OF HUNTINGTON, INDIANA

Huntington, located in Nuntington County in Northeast Indiana, has an invigorating climate because of the frequent changes of the weath-Pleasant, cloudless days ere interspersed with some rainy days throughout the yeer. Monsoon rains are unknown but rainfall is usually adequate in all seesons favoring a diversified agriculture. In the summer when moisture utilization is high, a dry month of below normal rainfall affects lewns, pastures, and crops.

Weather changes every few days come from the passing of weather fronts and associated centers of low and high eir pressure. In general, a high brings lower temperatures, lower humidity and aunny days. An approaching low brings increasing temperatures, increasing southerly wind, higher humidity, and commencement of rain or showers. This activity is greatest in the spring and least in late summer and early fall.

Precipitation is rather evenly distributed throughout the year, s heppy contrast to some sress of the United States that have s "dry season" and require irrigation to maintain green vegetation. The table of monthly rainfell for past years in this report shows the variation of rainfall that may be expected. There is a tendency for spring and early summer rains to exceed winter precipitation. The spring rains are very reliable insuring near maximum soil moisture going into summer when evaporation losses exceed rainfall and dry soils become more probable. A severe drought hes never been experienced. About one-third of the annual reinfall flows into streams and out of the area. Future needs may require conservation of this water.

The probability for unusually heavy rains in just a few hours is

indicated by a weather	study of the area:		
Frequency in 100 years	Rain in 1 hour	6 hours	12 hours
4	2.1	3.2	3.7
10	1.7	2.8	3.2
20	1.5	3 /.	2 8

Snowfall has varied reception. None occurs in the summer. Some winters have much snow and others have very little. An occasional snow storm may hamper travel and-clog roads but at the same time the snow blanket protects winter grains from the very cold sir that invariably follows. Heaviest snow storms are those out of the southwest. As they swirl northeastward, abundant moisture flows in from the Gulf of Mexico. A storm out of the northwest, with an inwerd flow of colder, drier air, leaves iess snow. Some mid-winters are thus cold but snowfall is normal or less.

Relative humidity is not measured at this station but estimates are possible from the climatology of the area. Relative humidity varies on sunny summer days from a percent in the 40's in the early afternoon to the 90's about sunrise. Relative humidity rises and falls much as temperature does during a typical day but the highest percent usually occurs with the minimum temperature and the lowest percent with the maximum temperature. front is next in importance in thanging relative humidity down-

Winds blow most frequently from the southwest, however, in one or two of the winter months, prevailing winds are northwest. Damaging winds heve three sources. In the order of diminishing area coverage but incressing intensity, they are: lows passing through the region, thunderstorms, and tornadors. Only 10 torna-dors have been reported in the County since 1916. Very few were of sufficient size to injure people and property. Thunderstorms including incidences of lightning and thunder, occur about 46 days of the year. Most of these occur in the spring and early summer. They are seldom so severe as to cause loss of life, property, or crops. Death dealing smog or fog is unknown.

Heating degree days in the above table provide a comparative number for calculating heating requirements between different places and different times. Fuel consumption for heating is proportional to degree day totals, so a month with twice the heating degree days of another month requizes twice as much fuel for heating. Degree days for a single day are obtained by subtracting the mean temperature from 65 degrees.

The growing season (defined here as the number of days between the last spring and first fall temperature of 32°) averages 155 days in length. The season is 176 days or more in 10% of the years, 166 days or more in 25% of the years, less than 144 days in 25% of the years, and less than 134 days in 10% of the years.

Many days of the year sre nearly ideal in temperature. days, in the summer when temperatures exceed 90, or decline below zero in the winter, tend to obscure this fact. The fall season is considered by many as the best time of year for outdoor activities. Spring is also a favorite season but actually this season has more days of rain and thunderstorms. In the fell the etmosphere in total seems fore quiet. Air and soil temperatures are nearer in agreement than any other time of the year, thus, convective activity is diminished. Hany days are sunny and showers are less frequent.

> Weather Sureau State Climatologist Purdue University, Agronomy Department Lafayette, Indiana



Table 2., Continued

Average Temperature (\*F)

(Inches)
pilation
Preci
Tola

		25.21	42.45	32.75	38.69	35.87	28.72 37.26 43.22 48.21	41.48 41.48 29.84 42.87 38.59	33.00 43.94 35.40 47.53 30.39	76.63 27.76 26.51
Dec		1.63	3.24	1.23	1.98	1.89	2.20 1.85 3.82 4.15 2.10	3.98 2.01 1.36 2.19 0.59	2.79 4.74 0.45 2.39 1.16	0.50
Nov.		3.32	2.99	3.12	2.98	4.47	2.18 2.12 4.06 1.25 4.51	3.22 2.72 1.79 1.79 4.43	2.71 1.92 4.31 2.82 1.37	2.64
Oct	3	0.93	3.10	4.12	2.03	2.77	3.24 2.63 2.18 6.07 1.68	3.64 0.53 1.37 8.55 6.66	0.62 4.04 0.83 3.78 1.71	2.50 2.57 0.28
Sept.	3	4.14	2.43	0.43	3.14	3.54	1.53 4.48 4.52 3.52 4.11	1.58 3.83 1.67 2.05 1.96	1.13 2.73 3.67 4.43 2.28	3.19
Aug.	-fand-	2.29	3.30	2.88	1.68	1.86	0.93 3.20 1.57 2.17 4.18	2.77 4.63 1.68 6.75 3.36	2.37 2.50 3.48 1.72 3.16	2.22 1.68 1.40
July	ć.,	1.97	3.66	3.66	2.14 6.24	1.26	2.02 2.65 3.21 3.69 2.95	3.70 2.21 4.18 5.00 6.24	3.02 3.91 6.23 2.01 2.92	4.93
lune	allin	1.94	5.91	3.15	3.11	0.44	3.24 3.94 5.15 7.02 4.47	6.79 3.47 2.22 3.93 2.60	4.14 7.52 9.43 6.94 4.00	4.64 1.89 2.82
×	May	0.89	4.17	0.93	2.94	6.95 4.95	6.02 4.47 4.76 5.12 2.21	3.76 6.47 3.18 2.91 1.98	5.95 4.05 2.38 4.85 4.54	2.11 4.09 2.94
Anr	Apr.	3.20	5.91	5.24	3.59	2.93 2.91 3.20	0.92 5.43 2.24 1.92 5.75	3.43 3.79 3.33 3.02 2.47	1.69 8.21 1.80 2.96 1.96	5.50 1.33 3.84 6.06
X X	INTOI.	3.03	2.72	3.24	3.73	2.58 3.81 6.81	2.79 2.50 5.45 2.27 2.68	3.63 5.16 5.02 1.76 5.44	3.32 1.28 0.93 2.96 1.47	4.19 2.69 5.02 4.82
F. da	reb.	1.18	1.79	3.46	3.61	2,29	1.80 0.49 2.82 2.94 4.32	3.24 2.56 1.57 2.59 1.32	4.00 1.17 1.16 3.67 3.00	2.40 2.49 1.23 1.44
1	Jan.	3.38	1.55	3.71	1.90	0.69	1.35 3.50 3.49 8.09 9.40	1.60 4.10 2.47 2.28 1.54	1.26 1.87 1.25 4.00 2.32	0.44 3.46 0.97 2.50
Y A	rear	1934	1936	339	141	1943 1944 1945	0561 1948 1948 1950	951 952 953 954 1955	956 957 958 959 960	961 962 963 964
11 '	'		2 2 3	5 5 5	-	19	2 2 2 2 2	9 9 9 9	199	
11	Ann	51.6 1 49.8 1		52.6 19 52.0 19 49.2 19		49.9 19 51.6 19 50.2 19	52.8 19 49.8 19 50.8 19	49.8 19 51.6 19 52.9 19 52.4 19	52.0 19 51.2 19 49.4 19 51.9 19 69.9 19	50.7 50.1 50.1 49.4
l'and			9.05		52.1					
Provide the second	Ann	51.6	2 26.3 49.6	52.6 52.0 49.2	.2 35.6 52.1 .8 25.4 50.4	49.9 51.6 50.2	52.8 49.8 50.8	49.8 51.6 52.9 52.4	52.0 51.2 49.4 51.9 49.9	50.7
M. D. C. Band	Dec. Ann	4 26.2 51.6 8 24.1 49.8	37.0 33.5 50.6 37.2 26.3 49.6	4 30.6 52.6 5 33.2 52.0 8 35.0 49.2	42.2 35.6 52.1 42.8 25.4 50.4	.0 27.4 49.9 .0 24.1 51.6 .4 23.8 50.2	29.6 49.8 23.6 49.8 23.6 50.8 521.7	28.9 49.8 13.1 51.6 14.8 12.3 52.9 14.3 52.4 17.5 52.4 17.5 52.4 17.6 17.6 17.6 17.6 17.6 17.6 17.6 17.6	35.9 52.0 35.6 51.2 22.3 49.4 36.1 51.9 25.6 49.9	27.7 24.5 50.1 19.7 69.4
N A. A	Nov. Dec. Ann	39.8 26.1 51.6 39.8 26.1 49.8	53.2 37.0 33.5 50.6 50.2 37.2 26.3 49.6	43.4 30.6 52.6 39.5 33.2 52.0 37.8 35.0 49.2	56.0 42.2 35.6 52.1 54.2 42.8 25.4 50.4	38.0 27.4 49.9 42.0 24.1 51.6 42.4 23.8 50.2	45.0 34.2 52.8 36.4 29.6 49.8 45.2 31.6 50.8 35.5 21.7	34.2 28.9 49.8 41.8 33.1 51.6 43.4 32.3 52.9 41.3 41.3 52.4 38.2 27.6 52.4	41.9 35.9 52.0 41.1 35.6 51.2 43.4 22.3 49.4 36.5 36.1 51.9 43.5 25.6 49.9	41.5 27.7 50.7 40.7 45.6 19.7 49.4
Total Control	Oct. Nov. Dec. Ann	54.0 44.4 26.2 51.6 51.6 39.8 24.1 49.8	68.0 53.2 37.0 33.5 50.6 63.0 50.2 37.2 26.3 49.6	56.0 43.4 30.6 52.6 54.4 39.5 33.2 52.0 56.3 37.8 35.0 49.2	69.8 56.0 42.2 35.6 52.1 62.5 54.2 42.8 25.4 50.4	52.0 38.0 27.4 49.9 52.6 42.0 24.1 51.6 51.6 42.4 23.8 50.2	\$8.6 45.0 34.2 52.8 60.5 36.4 29.6 49.8 50.2 45.2 31.6 50.8 58.0 58.2 35.5 21.7	56.4 34.2 28.9 49.8 48.2 41.8 33.1 51.6 57.1 43.4 32.3 52.9 56.6 41.3 41.3 52.4 55.3 38.2 27.6 52.4	59.3 41.9 35.9 52.0 50.5 41.1 35.6 51.2 54.7 43.4 22.3 49.4 53.7 36.5 36.1 51.9 54.2 43.5 25.6 49.9	55.8 41.5 22.7 50.2 56.5 40.7 24.5 50.1 61.4 45.6 19.7 49.4
N. D.	Sept. Oct. Nov. Dec. Anni	65.2 54.0 44.4 26.2 51.6 64.0 51.6 39.8 24.1 49.8	76.7 68.0 53.2 37.0 33.5 50.6 74.7 63.0 50.2 37.2 26.3 49.6	65.4 56.0 43.4 30.6 52.6 69.9 54.4 39.5 33.2 52.0 63.3 56.3 37.8 35.0 49.2	72.6 69.8 56.0 42.2 35.6 52.1 70.6 62.5 54.2 42.8 25.4 50.4	66.3 52.6 42.0 24.1 51.6 66.8 51.6 42.4 23.8 50.2	68.8         66.4         58.6         65.9         34.2         52.8           79.2         66.0         60.5         36.4         29.6         49.8           71.9         67.5         50.2         45.2         31.6         50.8           73.2         59.4         58.0         -         50.8           69.9         63.4         58.2         35.5         21.7         -	62.6 56.4 34.2 28.9 49.8 63.7 48.2 41.8 33.1 51.6 65.8 57.1 43.4 32.3 52.9 68.0 54.6 41.3 41.3 52.4 68.1 55.3 38.2 27.6 52.4	63.8 59.3 41.9 35.9 52.0 64.2 50.5 41.1 35.6 51.2 64.6 54.7 43.4 22.3 49.4 68.6 53.7 36.5 36.1 51.9 68.3 54.2 43.5 25.6 49.9	64.3 61.4 45.6 19.7 50.7 60.4 64.3 61.4 45.6 19.7
To Co	Aug. Sepl. Oct. Nov. Dec. Ann!	72.2 65.2 54.0 44.4 26.2 51.6 73.0 64.0 51.6 39.8 24.1 49.8	19.5         76.7         68.0         53.2         37.0         33.5         50.6           13.5         74.7         63.0         50.2         37.2         26.3         49.6	24.4     65.4     56.0     43.4     30.6     52.6       72.0     69.9     54.4     39.5     33.2     52.0       73.6     63.3     56.3     37.8     35.0     49.2	75.8 72.6 69.8 56.0 42.2 35.6 52.1 73.9 70.6 62.5 54.2 42.8 25.4 50.4	72.3         61.0         52.0         38.0         27.4         49.9           74.8         66.3         52.6         42.0         24.1         51.6           71.2         66.8         51.6         42.4         23.8         50.2	68.8         66.4         58.6         65.9         34.2         52.8           79.2         66.0         60.5         36.4         29.6         49.8           71.9         67.5         50.2         45.2         31.6         50.8           73.2         59.4         58.0         -         50.8           69.9         63.4         58.2         35.5         21.7         -	70.6     62.6     56.4     34.2     28.9     49.8       71.5     63.7     48.2     41.8     33.1     51.6       73.7     65.8     57.1     43.4     32.3     52.9       72.0     68.0     54.6     41.3     41.3     52.4       76.2     68.1     55.3     38.2     27.6     52.4	13.2     63.8     59.3     41.9     35.9     52.0       22.0     64.2     50.5     41.1     35.6     51.2       71.5     64.6     54.7     43.4     22.3     49.4       77.5     68.6     53.7     36.5     36.1     51.9       73.0     68.3     54.2     43.5     25.6     49.9	21.6     69.6     55.8     41.5     27.7     50.2       72.5     63.0     56.5     40.7     24.5     50.1       68.7     64.3     61.4     45.6     19.7     49.4
100	July Aug. Sept. Oct. Nov. Dec. Anni	80.0 72.2 65.2 54.0 44.4 26.2 51.6 76.7 73.0 64.0 51.6 39.8 26.1 49.8	69.0 79.5 76.7 68.0 53.2 37.0 33.5 50.6 68.6 73.5 74.7 63.0 50.2 37.2 26.3 49.6	73.8 72.0 65.4 56.0 43.4 30.6 52.6 73.8 72.0 73.6 95.4 36.3 37.8 33.0 49.2 73.0 73.6 63.3 56.3 37.8 37.8 35.0 49.2	70.0         75.8         72.6         69.8         56.0         42.2         35.6         52.1           70.2         73.9         70.6         62.5         54.2         42.8         25.4         50.4	74.4         72.3         61.0         52.0         38.0         27.4         49.9           74.9         74.8         66.3         52.6         42.0         24.1         51.6           72.0         71.2         66.8         51.6         42.4         23.8         50.2	68.9 73.8 68.8 66.4 58.6 45.0 34.2 52.8 67.0 70.0 79.2 66.0 60.5 36.4 29.6 49.8 69.5 73.2 59.4 58.0 73.2 59.4 58.0 73.5 70.6 69.9 63.4 58.2 35.5 21.7 -	72.5     70.6     62.6     56.4     34.2     28.9     49.8       76.3     21.5     63.7     48.2     41.8     33.1     51.6       75.0     73.7     68.8     57.1     43.4     32.3     52.9       75.0     72.0     68.0     54.6     41.3     41.3     52.4       78.7     76.2     68.1     55.3     38.2     27.6     52.4	73.1     73.2     63.8     59.3     41.9     35.9     52.0       73.9     72.0     64.2     50.5     41.1     35.6     51.2       73.1     71.5     64.6     54.7     43.4     22.3     49.4       73.3     77.5     68.6     53.7     36.5     36.1     51.9       71.2     73.0     68.3     54.2     43.5     25.6     49.9	72.5 71.6 69.6 55.8 41.5 27.7 50.7 71.4 72.5 65.0 56.3 61.4 45.6 19.7 49.4
To Co	June July Aug. Sept. Oct. Nov. Dec. Anni	76.8         80.0         72.2         65.2         54.0         44.4         26.2         51.6           66.6         76.7         73.0         64.0         51.6         39.8         24.1         49.8	63.8 69.0 79.5 76.7 68.0 53.2 37.0 33.5 50.6 60.1 68.6 73.5 74.7 63.0 50.2 37.2 26.3 49.6	68.4 73.8 74.4 65.4 56.0 43.4 30.6 52.6 72.7 73.8 72.0 65.9 54.4 39.5 33.2 52.0 71.0 74.6 63.3 56.3 75.8 75.0 73.6 63.3 56.3 77.8	62.6 70.0 75.8 72.6 69.8 56.0 42.2 35.6 52.1 61.2 70.2 73.9 70.6 62.5 54.2 42.8 25.4 50.4	74.6         74.4         72.3         61.0         52.0         38.0         27.4         49.9           74.4         74.9         74.8         66.3         52.6         42.0         24.1         51.6           67.5         72.0         71.2         66.8         51.6         42.4         23.8         50.2	58.2         68.9         73.8         68.8         66.4         58.6         45.0         34.2         52.8           57.0         67.0         70.0         79.2         66.0         60.5         36.4         29.6         49.8           59.5         69.5         73.8         71.9         67.5         50.2         45.2         31.6         50.8           62.6         72.9         76.6         73.2         59.4         58.0         -         -         -           62.6         73.2         59.4         58.0         -         -         -         -         -         -         -           62.7         76.6         69.9         63.4         58.2         35.5         21.7         -	68.4         72.5         70.6         62.6         56.4         34.2         28.9         49.8           74.5         76.3         71.5         63.7         48.2         41.8         33.1         51.6           73.6         75.0         73.7         65.8         57.1         43.4         32.3         52.9           73.3         75.0         72.0         68.0         54.6         41.3         41.3         52.4           67.4         78.7         76.2         68.1         55.3         38.2         27.6         52.4	11.7     13.1     13.2     63.8     59.3     41.9     35.9     52.0       70.9     13.9     12.0     64.2     50.5     41.1     35.6     51.2       65.2     13.1     71.5     64.6     54.7     43.4     22.3     49.4       11.1     73.3     77.5     68.6     53.7     36.5     36.1     51.9       67.6     71.2     73.0     68.3     54.2     43.5     25.6     49.9	45.3     56.6     68.0     72.5     71.6     69.6     55.8     41.5     27.7     50.7       49.8     66.9     70.4     71.4     72.5     63.0     56.5     40.7     24.5     50.1       51.5     58.5     70.4     73.0     68.7     64.3     61.4     45.6     19.7     49.4       51.6     64.8     64.8     64.3     61.4     45.6     19.7     49.4
	May June July Aug. Sept. Oct. Nov. Dec. Ann!	64.9 76.8 80.0 72.2 65.2 54.0 44.4 26.2 51.6 54.2 54.0 44.4 26.2 51.6 54.2 54.2 54.1 49.8	48.6 60.1 68.6 73.5 74.7 68.0 53.2 37.0 33.5 50.6 49.6	60.7 68.4 73.8 24.4 65.4 56.0 43.4 30.6 52.6 63.6 43.4 30.6 52.6 63.6 17.7 73.8 72.6 69.9 54.4 39.5 73.2 52.0 56.9 71.0 73.6 63.3 56.3 73.8 73.8 73.0 49.2	54.5 62.6 70.0 75.8 72.6 69.8 56.0 42.2 35.6 52.1 54.1 61,2 70.2 73.9 70.6 62.5 54.2 42.8 25.4 50.4	60.0 74.6 74.4 72.3 61.0 52.0 38.0 27.4 49.9 66.2 74.4 74.9 66.3 52.6 42.0 24.1 51.6 54.9 67.5 72.0 71.2 66.8 51.6 42.4 23.8 50.2	51.0         58.2         68.9         73.8         68.8         66.4         58.6         45.0         34.2         52.8           48.6         57.0         67.0         79.2         66.0         66.0         36.4         29.6         49.8           53.8         59.5         69.5         73.2         59.2         45.2         31.6         50.8           48.4         62.6         72.9         76.6         69.9         63.4         58.2         35.5         21.7         -           43.9         67.3         68.2         36.2         34.2         31.6         50.8	61.6 68.4 72.5 70.6 62.6 56.4 34.2 28.9 49.8 58.7 74.5 75.3 71.5 63.7 48.2 41.8 33.1 51.6 62.8 58.4 41.8 33.1 51.6 62.8 52.8 57.1 43.4 32.3 52.9 56.4 56.8 57.1 43.4 32.3 52.9 56.4 57.8 57.1 43.4 57.3 52.9 56.8 57.1 68.0 54.6 41.3 41.3 52.4 52.4 57.8 68.0 54.6 55.3 38.2 27.6 52.4	61.2 71.7 73.1 73.2 63.8 59.3 41.9 35.9 52.0 61.0 70.9 73.9 72.0 64.2 50.5 41.1 35.6 51.2 60.1 65.2 73.1 71.5 64.6 54.7 43.4 22.3 49.4 65.3 71.1 73.3 77.5 68.6 53.7 36.5 36.1 51.9 58.5 67.6 71.2 73.0 68.3 54.2 43.5 25.6 49.9	56.6     68.0     72.5     71.6     69.6     55.8     41.5     27.7     50.7       66.9     70.4     71.4     72.5     63.0     56.5     40.7     24.5     50.1       58.5     70.4     73.0     68.7     64.3     61.4     45.6     19.7     49.4
	Apr. May June July Aug. Sept. Oct. Nov. Dec. Ann!	48.8 64.9 76.8 80.0 72.2 65.2 54.0 44.4 26.2 51.6 46.1 54.2 66.6 76.7 73.0 64.0 51.6 39.8 24.1 49.8	41.4 45.9 63.8 69.0 79.5 76.7 68.0 53.2 37.0 33.5 50.6 33.8 48.6 60.1 68.6 73.5 74.7 63.0 50.2 37.2 26.3 49.6	51.2 60.7 68.4 73.8 74.4 65.4 56.0 43.4 30.6 52.6 45.6 65.6 45.7 56.9 17.0 74.0 73.6 63.3 56.3 37.8 35.0	32.8 54.5 62.6 70.0 75.8 72.6 69.8 56.0 42.2 35.6 52.1 39.6 54.1 61,2 70.2 73.9 70.6 62.5 54.2 42.8 25.4 50.4	46.5         60.0         74.6         74.4         72.3         61.0         52.0         38.0         27.4         49.9           47.0         66.2         74.4         74.8         66.3         52.6         42.0         24.1         51.6           52.2         54.9         67.5         72.0         71.2         66.8         51.6         42.4         23.8         50.2	49.7         51.0         58.2         68.9         73.8         68.8         66.4         58.6         45.0         34.2         52.8           31.8         48.6         57.0         67.0         70.0         79.2         66.0         60.5         36.4         29.6         49.8           38.7         53.8         59.5         69.5         73.2         56.5         73.2         50.2         45.2         31.6         50.8           39.8         48.4         62.6         72.9         76.6         73.2         59.4         58.0         50.2         34.2         51.8           33.8         43.9         62.3         68.9         63.4         58.2         35.5         21.7         -	47.7         61.6         68.4         72.5         70.6         62.6         56.4         34.2         28.9         49.8           50.6         58.7         28.7         48.2         41.8         33.1         51.6           45.9         62.8         73.7         65.8         57.1         43.4         32.3         52.9           55.4         56.4         73.3         75.0         73.7         65.8         57.1         43.4         32.3         52.9           57.1         66.8         56.4         56.0         56.0         54.6         41.3         41.3         52.4           57.3         62.8         67.4         76.2         68.1         55.3         38.2         27.6         52.4	48.9         61.2         71.7         73.1         73.2         63.8         59.3         41.9         35.9         52.0           51.0         61.0         70.9         73.9         72.0         64.2         50.5         41.1         35.6         51.2           51.7         60.1         65.2         73.1         71.5         64.6         54.7         43.4         22.3         49.4           51.4         65.3         71.1         73.3         77.5         68.6         53.7         36.5         36.1         51.9           53.9         58.5         67.6         71.2         73.0         68.3         54.2         43.5         25.6         49.9	45.3     56.6     68.0     72.5     71.6     69.6     55.8     41.5     27.7     50.7       49.8     66.9     70.4     71.4     72.5     63.0     56.5     40.7     24.5     50.1       51.5     58.5     70.4     73.0     68.7     64.3     61.4     45.6     19.7     49.4       51.6     64.8     64.8     64.3     61.4     45.6     19.7     49.4
	Mar, Apr. May June July Aug. Sepl. Oct. Nov. Dec. Ann!	33.4 48.8 64.9 76.8 80.0 72.2 65.2 54.0 44.4 26.2 51.6 43.8 46.1 54.2 66.6 76.7 73.0 64.0 51.6 39.8 24.1 49.8	18.9 41.4 45.9 63.8 69.0 29.5 76.7 68.0 53.2 37.0 33.5 50.6 28.7 33.8 48.6 60.1 68.6 73.5 74.7 63.0 50.2 37.2 26.3 49.6	44.9 51.2 60.7 68.4 73.8 74.4 65.4 56.0 43.4 30.6 52.6 52.6 53.5 59.2 54.6 65.7 65.9 54.6 69.9 54.4 57.7 57.8 57.0 57.0 69.9 54.4 56.3 37.8 37.8 56.9 57.0 56.9 57.0 57.0 57.0 57.0 57.0 57.0 57.0 57.0	25.7 32.8 54.5 62.6 70.0 75.8 72.6 69.8 56.0 42.2 35.6 52.1 24.4 39.6 54.1 61.2 70.2 73.9 70.6 62.5 54.2 42.8 25.4 50.4	35.6         46.5         60.0         74.6         74.4         72.3         61.0         52.0         38.0         27.4         49.9           34.6         47.0         66.2         74.4         74.9         74.8         66.3         52.6         42.0         24.1         51.6           49.8         52.2         54.9         67.5         72.0         71.2         66.8         51.6         42.4         23.8         50.2	31.2         49.7         51.0         58.2         68.9         73.8         68.8         66.4         58.6         45.0         34.2         55.8           21.5         31.8         48.6         57.0         67.0         70.0         79.2         66.0         66.5         36.4         29.6         49.8           28.1         38.7         53.8         59.5         69.5         73.8         71.9         67.5         50.2         45.2         31.6         50.8           32.7         39.8         48.4         62.6         72.9         76.6         79.4         58.0         50.2         45.2         31.6         50.8           33.7         43.9         62.3         76.6         69.9         63.4         58.2         35.5         21.7         -	37.3         47.7         61.6         68.4         72.5         70.6         62.6         56.4         34.2         28.9         49.8           36.9         50.6         58.7         24.5         76.3         71.5         63.7         48.2         41.8         33.1         51.6           40.2         45.9         62.8         73.6         75.0         73.7         65.8         57.1         43.4         32.3         52.9           35.6         55.4         56.4         73.3         75.0         72.0         68.0         54.6         41.3         41.3         52.4           39.7         57.3         62.8         67.4         78.7         76.2         68.1         55.3         38.2         27.6         52.4	38.2     48.9     61.2     21.7     23.1     23.2     63.8     59.3     41.9     35.9     52.0       38.9     51.0     61.0     70.9     73.9     72.0     64.2     50.5     41.1     35.6     51.2       36.1     51.7     60.1     65.2     73.1     71.5     64.6     54.7     43.4     22.3     49.4       37.8     51.4     65.3     71.1     73.3     77.5     68.6     53.7     36.5     36.1     51.9       25.9     53.9     58.5     67.6     71.2     73.0     68.3     54.2     43.5     25.6     49.9	42.4         45.3         56.6         68.0         72.5         71.6         69.6         55.8         41.5         27.7         50.2           35.9         49.8         66.9         70.4         71.4         72.5         63.0         56.5         40.7         24.5         50.1           41.6         51.5         58.5         70.4         73.0         68.7         64.3         61.4         45.6         19.7         49.4           37.8         51.6         64.8         64.3         61.4         45.6         19.7         49.4

# STATION HISTORY

been located 1.1 miles northcast of the past office in liuntington, Indiana, since June 1, 1954.

Earlier observers, dates all service, and location of station are: William McGrey, November 1, 1893 to January 31, 1966; Charles McGrey, February 1, 1906 to May 31, 1915, 153 N. Jefferson Street; C. Hirace Kiracnfe, June 1, 1915 to August 31, 1924, 349 W. Tipton Street; Ivan 0. Murphy, January 1, 1973 to August 12, 1978, 803 Olinger Street; Carl F. Ogle, August 24, 1928 to November 30, 1928, 18 M. Jefferson 1, 1928, 18 M. Jefferson 1, 1929 to May 31, 1954, 231 Vine Street. This study of local climate is possible because a citizen of the community for many years generously donated a few minutes a day, seven days a week, reading and recording weather information from government instruments. The present observer is George P. Dolby. His weather station has

# EXTREMES AND DATES OF OCCURRENCE (1893-1963)

	=	i pilitrat.	1.	18.101	Grente	rat Daily	Grentent	. Monthly
fonth	Ten	Temperature	Tem	Cemperature	Prec	Precipitation	Snow	Snowfall
Jan.	99		-20	1/23/36	2.16	1/3/50	21.9	1895
eh.	70		-18	2/2/31	2.52	2/24/36	24.5	1900
far.	P.4.		8-	3/12/48	2,88	3/14/25	28.0	1899
. zdi	16	-	14	4/12/40	1.85	4/11/44	15.2	1961
fay	6		24	5/9/67	3,52	2/1/96	3.5	1923
luna	106	_	35	6/3/45	90.9	9/23/00		
July	110		42	1/20/41	3,65	7/31/42		
W.	105	_	35	8/30/46	3.93	8/1/29		
inpt.	103	•	26	9/29/51	1,63	9/3/32	ŀ	1917
361.	3/6		1.5	10/22/26	3,22	10/12/01	3.5	1950
Nov.	8	11/11/10	- 5	11/25/50	1.93	11/7/25	12,5	1950
Dr.c.	68		-15	12/16/51	1.94	12/21/18	17.0	1903

# PROBABILITY OF LOW TEMPERATURES IN SPRING AND FALL

Temp.		Percent after th	Percent of accurrence after the date in spring	rrence n spring			Percen	Percent of accurrence before the date in [all	in fall	
	300%	757	20%	25%	107	107	252	20%	757	206
07	5/18	5/25	6/2	01/9	21/9	6/5	6/6	9/17	9/25	10/2
36	2/4	5/10	5/17	5/24	5/30	9/15	9/21	9/27	10/3	10/9
32	4/22	4/29	3/6	5/13	\$/20	9/23	01/6	10/8	10/16	10/3/
28	9/9	4/13	4/22	5/1	S/H	10/5	10/17	10/31	10/29	11/6
24	3/18	3/28	4/7	4/17	4/27	10/70	10/57	11/4	11/12	11/11
20	3/6	3/15	1/54	4/2	11/7	10/27	11/4	11/12	11/20	11/28
16	2/24	1/1	1/17	1/21	1728	11/0	11/18	11/28	1.7/R	11/1

This table summarizes for a 30-year period the dates when fou temperatures such as 12%, last or-curred in the fall. The average date is given in the fall edines. The table shows that the last temperature of 32° or lower in the surfame occurs after May 11 in 3% of the years, and before September 30 in the fall. Frohald little for other temperatures are such cated. Reference: "Blake of Freezing Temperatures.-Spring and Fall in indiana," by L. A. Schail, J. E. Newman, and F. II. Emerson.



## Physiography

Huntington County is located entirely within the Tipton Till Plain physiographic region of the State of Indiana (6). With respect to North American physiography, it lies in the Till Plains section of the Central Lowlands Province. A physiographic map of Indiana is shown in Figure 3.

## Topography

The topography of Huntington County is generally nearly level to strongly sloping north of the Little Wabash River and nearly level to moderately sloping in the southern part of the county. The nearly level terrain of the till plain is broken by the Wabash River, the Little Wabash River, and the Salamonie River and their tributaries and by two ridge moraines which cross the county. Local relief along the three major river valleys is much as 90 feet (7), while relief in the morainic areas usuas ally does not exceed 20 to 25 feet locally. Topography of the ridge moraines varies from the more common gently undulating swell and sag type to the rolling relief of knob and basin topography in some places. Elevation reaches a maximum of 912 feet above mean sea level in the northwest corner of the county (2). A minimum elevation of 660 feet is located where the Wabash River exits the county at the Wabash county line.

The most prominent topographic feature of Huntington county is the broad, relatively flat valley of the Little Wabash River,



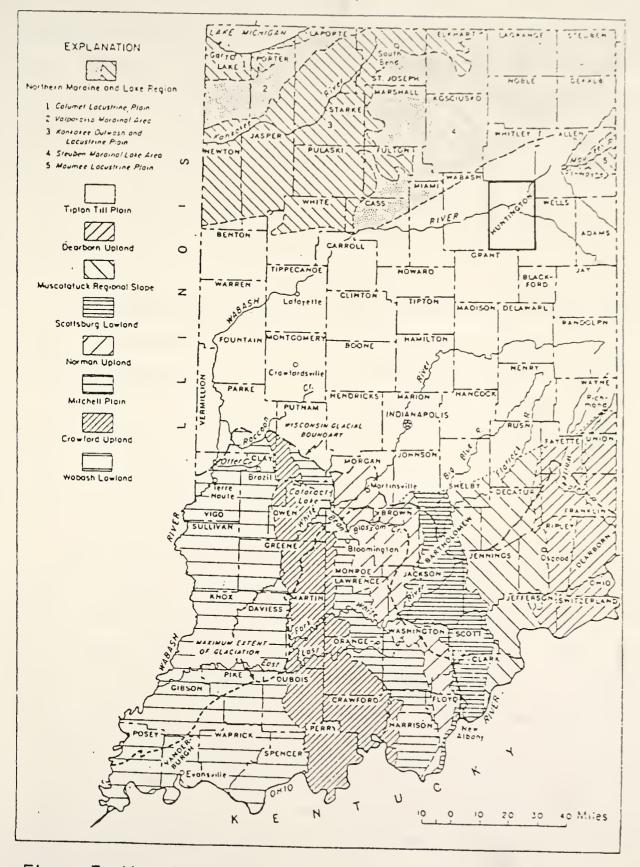


Figure 3. Map Showing Surficial Physiography of Indiana and Location of Huntington County (6)



sometimes referred to as the Maumee Sluiceway, through which large volumes of meltwater once flowed. The present-day Wabash River follows the courses of the sluiceway westward from its junture with the Little Wabash about 2.5 miles west of the City of Huntington. A topographic map of Huntington County is shown in Figure 4.

### Drainage

Huntington County lies entirely in the Wabash River Drainage basin of Indiana (5). The northeast part of the county lies in the Little Wabash River subdivision, while the southwestern part is drained by the Salamonie River Subdivision. A small area in the northwest corner of the county lies in the Eel River subdivision of the Wabash River drainage basin. The remainder of the county drains directly into the Wabash River.

The Little Wabash River is an underfit (narrow relative to width of valley) stream which flows through a wide glacial melt-water channel. Its course was dredged in many places northeast of Mardenis to improve sluggish drainage and was confined by shallow limestone bedrock further on before joining the Wabash River west of the City of Huntington. The Salamonie River is somewhat entrenched and exhibits several large meanders east of Mt. Etna. The Little Wabash and Salamonie Rivers flow through rather deep (up to 90 feet), well established valleys whereas the Wabash River flows through a relatively shallow (less than 50 feet deep), though well defined valley before entering the old



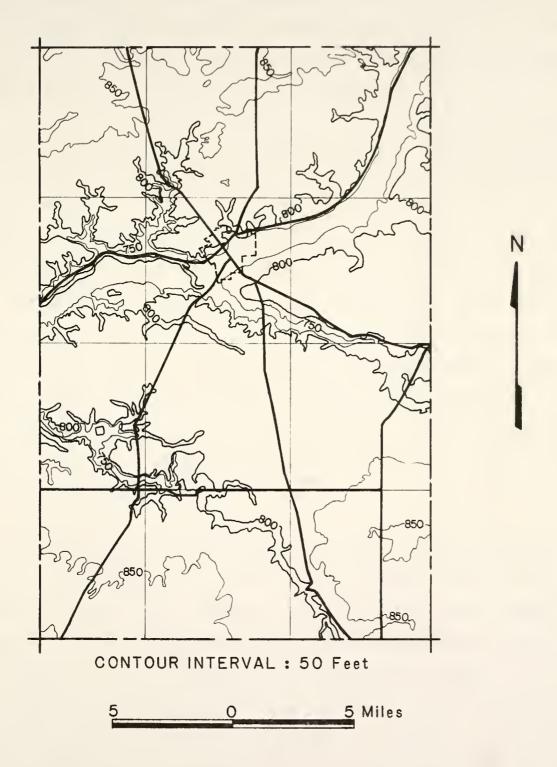


Figure 4. Topographic Map of Huntington County, Indiana (15)



meltwater channel. Shallow limestone bedrock encountered in places by these rivers apparently imposed little control on the stream courses, however, rates of erosion and depositional patterns were definitely modified to some degree.

Numerous local watershed divides are more or less defined by ridge moraines that pass through Huntington County, disrupting a generally dendritic regional pattern of drainage which is shown in Figure 5. The flow of several streams including Loon, Pony, and Clear Creeks appears to be deflected or directed to some extent in places by the ridge moraines. Loon Creek flows nearly parallel to the Wabash River for over ten miles before joining it due in part to a narrow, roughly east—west trending band of ridge moraine. Tributaries of the major streams flowing from areas of ridge moraine in the county are commonly shorter and more numerous than those from other areas due primarily to the more steeply sloping terrain.

The meanders along the Salamonie River are apparently due in part to the presence of a small patch of ridge moraine lodged between the river and Majenica Creek. The ridge moraine apparently impeded the river's flow to the Wabash River and, in effect, backed it up. Tributaries of the Salamonie River as it enters Huntington County are closely spaced and nearly parallel, taking on an almost trellis-like pattern of drainage. Drainage in the ground moraine is generally sluggish and dendritic while that in areas of knob and basin topography within the ridge moraines is often sluggish and somewhat deranged. Streams were



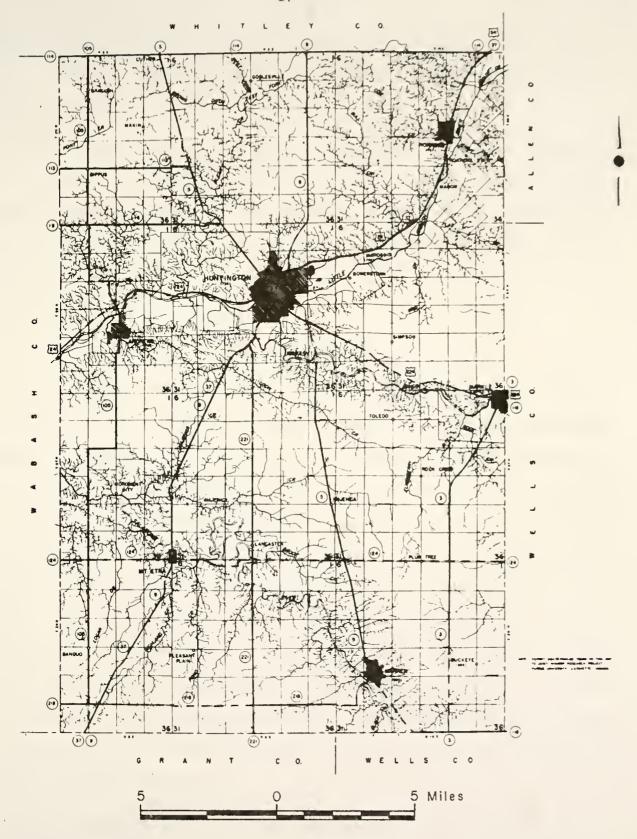


Figure 5. Drainage Map of Huntington County(5)



dredged and trenches excavated in order to improve drainage in these areas and on the broad, flat Maumee River sluiceway valley floor as well.

No natural lakes are found in Huntington County, however, both natural and man-made ponds are numerous (5). As previously stated, two flood control reservoirs are located in Huntington County; the Salamonie Reservoir on the Salamonie River and Huntington Reservoir on the Wabash River.

# Glacial Geology

The surficial glacial geology of Huntington County, Indiana consists of till and meltwater deposits of Wisconsinan age. Deposits of Wisconsinan age overlie any materials of Illinoian and Kansan age that may be present as well as those of any earlier glacial episodes. Wisconsinan age deposits include ridge and ground moraine, outwash and sluiceway sands and gravels, shallow or slackwater lacustrine deposits and some small, isolated patches of eolian sands north of the Little Wabash meltwater channel. The only surficial materials not of Wisconsinan age are recent alluvial and organic deposits as well as some shallow or slackwater lacustrine sediments. Silurian age limestone bedrock outcrops along the Wabash, Little Wabash, and Salamonie Rivers, and Rock Creek (8).

The Salamonie moraine (named after the river), passes in a discontinuous, somewhat arc-like fashion from the northwestern to



the southeastern parts of Huntington County while the Mississinewa moraine crosses the northwest and southwest corners of the
County (6). Both moraines were formed by the Erie Lobe of the
Wisconsinan ice sheet (7). The ridge moraines are generally more
rugged and are somewhat coarser in texture then the surrounding,
relatively flat and featureless ground moraine. The Salamonie
moraine is one of the least well defined ridge moraines formed by
the Erie lobe in Indiana, however, relief of 20 to 30 feet is not
uncommon near the Whitley county line.

Drift thickness in Huntington county (see Figure 6) ranges from less than one foot where bedrock outcrops along the major river valleys to more than 400 feet in the southwest part of the county along the Grant County line. Unconsolidated materials are generally less than 100 to 150 feet thick and limestone bedrock less than 10 to 20 feet from the surface in several places based on roadway borehole logs and other information (9). till is composed primarily of unsorted clay, sand, and silt with lesser amounts of gravel and cobble and boulder-sized rock frag-Thick lenses of sand and gravel are incorporated in the ments. till and are most common between the deposits of the earlier Tazewell and later Cary sub-ages of the Wisconsinan glacial period. Most of the tills at the surface in Huntington County are deposits of the Cary sub-age, although Tazewell age till is exposed along several bluffs of tributary streams to the Salamonie River near the Wabash County line (10). The thickest drift, located along the southern county line, is associated with



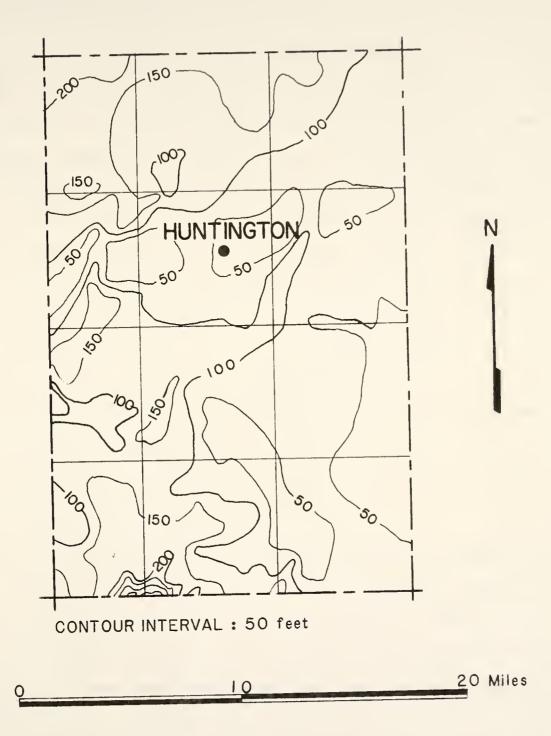


Figure 6. Unconsolidated Materials Thickness Map of Huntington County, Indiana (9)



a tributary of the preglacial Teays bedrock river valley (5).

The most distinctive glacial feature in the county is the previously mentioned meltwater channel associated with the present course of the Little Wabash River and the Wabash River. The channel sweeps in an arc from the northeast corner of the county southwestward, passing through the City of Huntington and exits the county about half way up the western county line where the Wabash River follows it to the Ohio River. Sometimes referred to as the Wabash or Maumee Sluiceway (10), the channel is up to two and one-half miles wide, in some places, and local relief along the channel wall of as much as 80 to 90 feet is not uncommon (5). The valley of the Wabash River upstream from its juncture with the Little Wabash River is thought to have been eroded primarily by the Wabash River itself and is, in contrast, rarely more than one half of a mile in width and local relief is not more than 50 feet along the valley wall.

The geologic history of the Wabash meltwater channel is rather complex and unique. The valley contains three well defined levels: an upper or Mississinewa terrace; a lower terrace called the Maumee terrace, and the lowest level which is the flood plain of recent age (10). The upper Mississinewa terrace was formed by sand and gravel-bearing meltwater during the late Tazewell and early Cary Wisconsinan glacial sub-ages. The lower Maumee terrace was carved out of the earlier Mississinewa outwash materials by the flood waters that escaped from glacial lake Maumee when it topped the ridge moraine dam that contributed to its



formation near the City of Fort Wayne. The lowest or flood plain level was eroded in recent time by the post-glacial Wabash and Little Wabash Rivers. The two terrace levels were distinct all the way to the mouth of the Wabash River (11).

The meltwaters of the Maumee or Wabash sluiceway eroded the overlying drift and cut a channel into the underlying Silurian age limestone/dolomite bedrock as much as 15 to 20 feet in places (12). The same sort of situation occurred along the much smaller Salamonie sluiceway, only to a much less extent. The flood and meltwaters of the so-called Wabash sluiceway apparently scoured the valley floor to a somewhat deeper depth from the northeast corner of the county to about three miles east of Huntington near Mardenis where rapid erosion was impeded by limestone/dolomite bedrock. When the flood and meltwaters abated, water apparently backed up behind the slightly higher bedrock valley floor forming a shallow or slackwater lake in which lacustrine silts and clays were deposited over any underlying glacio-fluvial sands and gravels. This interpretation is strictly the author's and is based on information obtained from the SCS Soil Survey of Huntington County (2) and roadway borehole information as well as information obtained from other sources of literature during previous studies.

#### Bedrock Geology

Huntington County, Indiana is underlain primarily by shale, limestone, and dolomite bedrock of Silurian age (7). Ordovician



age limestone and shale is found at the bedrock surface in a deep, preglacial Teays River tributary valley in the southwest part of the county (see Figure 7). Sandstone and limestone of Devonian age lies beneath the northern county line.

Huntington County is located in the Bluffton Plain bedrock physiographic unit of Indiana as shown in Figure 8 (13). The Bluffton Plain exhibits topography typical of a well dissected peneplain (see Figure 9) with intervalley bedrock surface elevation of about 700 to 800 feet above mean sea level. Beds dip regionally less than five degrees to the north away from the Cincinnati Arch (7). Bedrock structure, as defined by the surface of the Trenton Formation, is shown in Figure 10.

Limestone and dolomite are exposed at the surface in numerous places in the Wabash River and Little Wabash River valleys, and in some places along the valleys of the Salamonie River and Rock Creek (7) (12). A limestone bench is found near the surface about one mile southeast of the town of Warren in Huntington County along the Salamonie river. The bench bears the symbol of thin outwash, recent alluvium, and residual soil over shallow limestone-dolomite bedrock on the engineering soils map which accompanies this report. Limestone is exposed along the Wabash River near the town of Markle where a quarry is located on the tributary Rock Creek about one mile south of the town. Limestone first appears along the Little Wabash River near the town of Mardenis and is exposed nearly continuously to a point about three miles west of the junction with the Wabash River where it



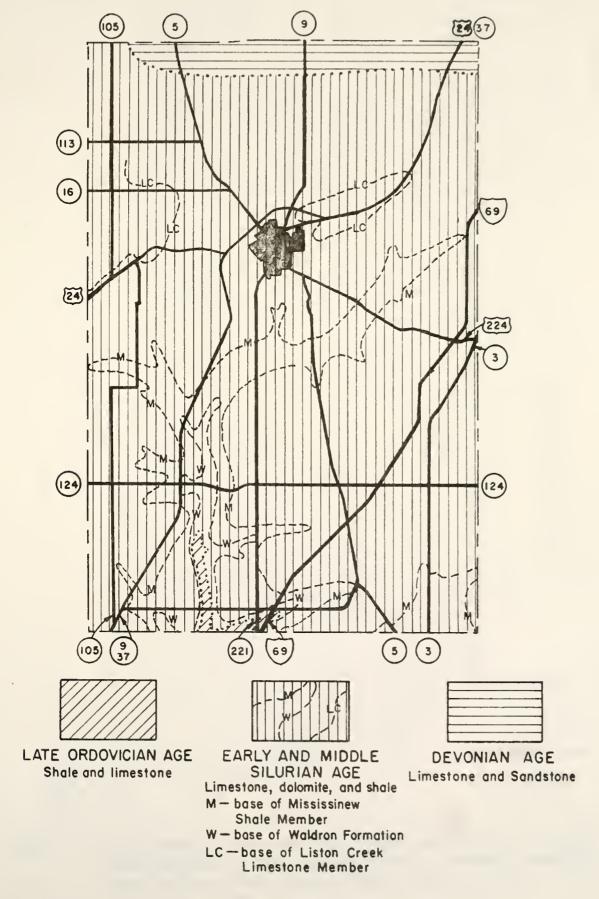


Figure 7. Geologic Map of Huntington County (16)



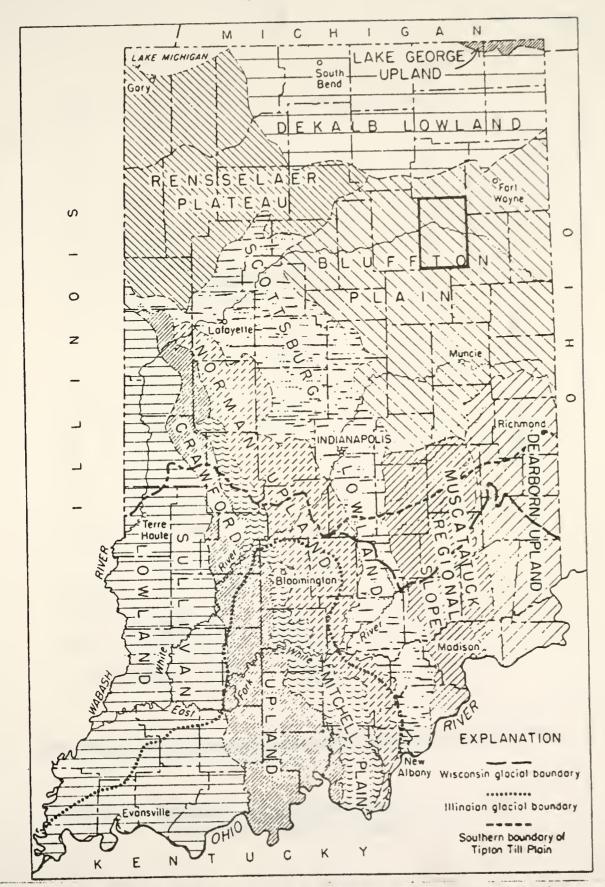
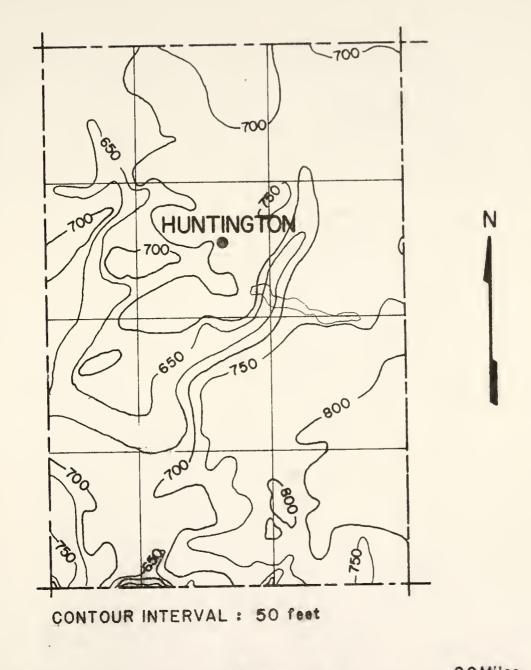


Figure 8. Map Showing Bedrock Physiographic Units of Indiana and Location of Huntington County. Slightly Modified from Indiana Geol. Survey Rept. Prog. 7, fig. 3 (13)





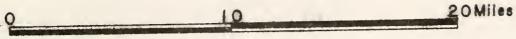


Figure 9. Bedrock Topography Map of Huntington County, Indiana (17)



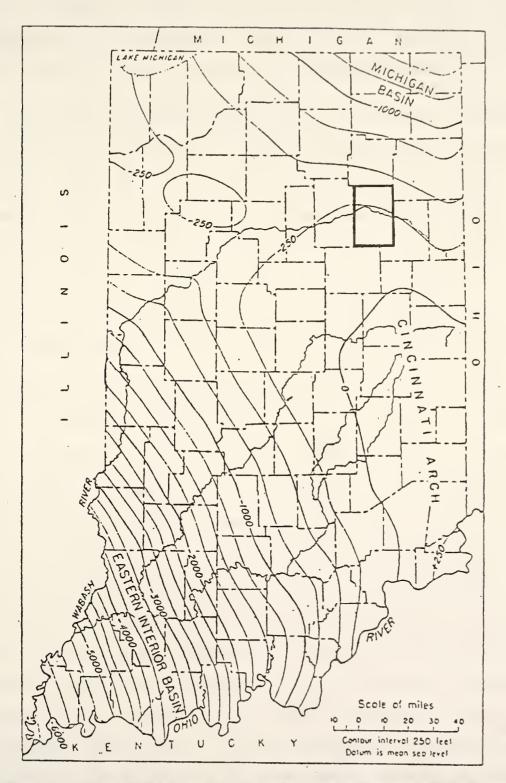


Figure 10. Map of Indiana Showing Regional Bedrock Structure as Defined by Surface of Trenton Limestone and Location of Huntington County (7)



disappears again beneath about 10 to 15 feet of drift. Limestone bedrock reappears about a mile or so downstream and is exposed intermittently to the Wabash County line. Another quarry is located about two miles northeast of downtown Huntington.

The limestone exposed along the old Maumee Sluiceway is apparently at the crest of a small anticline known as the Wabash Arch (14). Beds dip away to the north and south from the valley at about 45°. Erosion of the bedrock has occurred in on almost breached-anticline fashion. Bedding is massive near the town of Mardenis, becoming thinner to about two inches toward the Wabash County line. The limestone observed at the surface close to the Wabash County line was highly fractured and deeply weathered.

Several small bioherm reefs called klintar (11) are exposed along the Wabash River valley near the western county line. These reefs vary in size from a few hundred acres to less than five acres. A small klint (singular) was encountered by the author on US 24 about 300 yards west of county road 900 west. The reefs are generally dome-shaped and are composed of a massive, unstratified, dolomitic core of stromatoporoid, coral, bryozoan, and algae remains. The flank beds dip about 45 to 65 degrees near the core, flattening to about three degrees some distance away from the center. The flank beds are highly fractured and contain numerous faults with slickensides. The reefs, particularly the cores, are very resistant to erosion and were consequently left exposed by the meltwaters which scoured away the more easily eroded drift and the underlying, `softer´



limestone that surrounds the reefs. Numerous klintar are found along the Wabash River valley in neighboring Wabash County, an area recognized as the 'type location' of these features by many geologists.

Shale benches were found along the Wabash River in Wabash County (11), however, no pedalogical soils found in Huntington County were supposedly underlain by shale according to the SCS soil survey and no shale was found exposed at the surface by the author. Ward(12) writes of a dolomitic shale exposed intermittently along the Wabash River east of the junction with the Little Wabash River. The author did note an increase in clay content in the limestone or dolomite toward the Wabash County line as evidenced by the thinner bedding associated with clayey laminae observed in some Wabash River tributary valleys.



## GENERAL MAPPING METHOD

#### ENGINEERING SOIL AREAS

The preliminary steps of the mapping procedure included assembling a photomosaic of Huntington County and marking the county lines and section corners on the mosaic boards. Engineering soil map boundaries of adjacent counties were then located along the county lines and the land form - parent material associations identified. The actual mapping began with the flood plains and proceeded upstream from the Wabash County line. Mapping progressed upward through the terrace deposits into the upland areas of ridge and ground moraine and their associated depressional and stream deposits. The soil boundaries were identified by stereoscopic inspection of the land forms and by surface soil texture as revealed by phototones. The soil boundaries were marked on the mosaic.

The second main phase of the mapping procedure involved grouping of the SCS pedalogical soil series according to land form and parent material and identifying these areas on the agricultural map sheets using a color-code. Preliminary soil boundaries on the photomosaic were then compared with the boundaries on the map sheets and modified as necessary after analytical reexamination of the aerial photographs. Further boundary adjustments were made based on information obtained in the field.



Thirdly, the soil boundaries were transferred from the pictures to a pencil-copy base map using a mechanical reducing device. The scale was reduced from approximately three inches to the mile on the photos to one inch to the mile on the base map. The land form - parent material association's were identified on the pencil base map using a color and symbol code.

The final phase of the mapping procedure was the drafting of the master copy. The engineering soil boundaries were traced from the pencil copy in ink onto the master copy by a draftsperson. The land forms were then identified on the master copy using the standard set of symbols developed for the mapping project. Surface soil texture, (ie., relative composition of sand, silt, clay, etc.), was then superimposed on the land form parent material associations using the symbols shown in the map's legend. General soil profiles of the engineering soils in Huntington County are shown on the left-hand side of the engineering soils map.

The following discussion is a brief explanation of the land form - parent material areas delineated on the preliminary engineering soil map and the engineering characteristics of the soils associated with the topographic forms within the areas.

# Glacial Till Deposits

# Ridge Moraine

Parts of the Salamonie and Mississinewa ridge moraines, formed by the Erie Lobe of the Wisconsinan ice sheet, are found



in Huntington County. These moraines generally coincide with the local watershed divides and for the most part are gently rolling, not exhibiting the characteristic rugged topography associated with ridge moraines. There are areas in the north-central part of the county and south of a narrow, generally east-west trending the Salamonie moraine in the central part of the county where the terrain more closely resembles the hummocky topography typical of many ridge moraines. Small areas of knob and basinlike topography where relief may exceed 40 feet locally are found in these locations, and deposits of peat and muck are more numerous than elsewhere. Relatively coarser textured knolls (i.e., more sand) are more common in the ridge moraines than in the ground moraine as evidenced in the field, however, there is no apparent relationship between the distribution of probable kames and the ridge and ground moraine, nor is there any such relationship with deposits of peat and muck and highly organic topsoil, with the exception of the two areas previously mentioned. Local relief is generally on the order of 20 to 30 feet in the ridge moraines in Huntington County, Indiana.

The same soil series developed on both the ground and ridge moraine in Huntington County, however, the distribution of these soils between the two land forms shows a marked contrast which is attributed primarily to general differences in topography rather than a substantial variance in parent material (18). The Blount and Pewamo soil series by far account for the greatest areal extent of the land surface in both the ridge and ground moraine,



the former occupying elevated positions in the terrain and the latter the lower-lying areas (2). The Pewamo soil series is more extensive in the ground moraine and soil areas are relatively large, while soil areas in the ridge moraines are smaller and are about equally distributed between the Pewamo series and the Blount and other soil series based on the SCS soil map sheets. Other soils developed on the ridge moraines in Huntington County include the Rawson Variant and Glynwood series on convex rises and knolls and the Haskins Variant and Morley series on intermediate positions (2). These soils are also found in areas of ground moraine but to a much less extent, presumably due to less differentiation of the soils based on topography in the nearly level ground moraine.

The soils developed on knolls and swells in the ridge moraines in Huntington County include the Blount, Glynwood, and Rawson Variant pedalogical soil series (2). The Blount and Glynwood series are characterized by a silty loam (A-4 to A-6) surface soil which extends to a depth of about eight inches. Beneath eight inches is found a silty clay-loam or clay loam (A-4 to A-7). The Rawson Variant soil series is characterized by a sandy loam (A-2 to A-4) soil to a depth of about 35 inches. Beneath the sandy loam is found a clay loam (A-6 to A-7). Samples taken in the field from ridge moraine swells revealed a sandy surface soil which was underlain by a silty clay-loam type soil at a depth of about 10 inches to about 15 to 25 inches. A silt loam soil was found beneath to a depth of about 30 inches.



This description is only general and is based on hand examination of a limited number of field samples.

Low-lying areas in the ridge moraines are usually connected in a network of sluiceways and draws with few isolated swales. The dominant soil series developed on the lower topographic positions is the Pewamo as determined from the SCS map sheets. Isolated areas of the Patton (Pe variation, see Appendix A-1) and Houghton (organic) soil series are found in the deeper depressions. These soils developed in deposits of shallow-water lacustrine sediments and organic matter, discussed separately in the text under 'Depressional Deposits'. The Haskins Variant soil series is found in close association with the Pewamo series and was referred to in the development of the general soil profile for 'Low' areas in the ridge moraines shown on the left-hand side of the engineering soils map of Huntington County.

The Pewamo soil series developed most widely in the low topographic positions and is characterized by a silty clay-loam (A-6 to A-7) soil with a few pebbles throughout the soil profile (2). The Haskins Variant series developed on slightly sloping (1 to 4 percent) ground adjacent to Pewamo soils and is characterized by a fine sandy loam (A-4) surface soil to a depth of about 10 inches. The surface soil is underlain by a sandy loam (A-2-4 to A-4), a loam (A-4 to A-6) soil, or a silty clay-loam (A-6) to a depth of about 31 inches beneath which is found a clay loam (A-6) with some gravel. The percent areal distribution of the ridge moraine soils is given in Table 3 along with the



TABLE 3. ACREAGE AND PROPORTIONATE EXTENT OF THE SOILS

	Soil name	Acres	Percent
symbol			
	and the state of t	7/7	0.2
ApA	Cambon to the personal and	-1 92,579	37.1
BcB2	1 to 4 percent atopes;	18	0.1
ChB	and, 5 to 12 percent stop	2.622	1.1
E e	silt loam, occasional	,31	•
PoA	to 2 percent	206	0.2
POB	2 to 6 percent slopes	200	-
2000	loam, 6 to 12	y u	10
200	11t loam occasio	ğ.	7 -
200	in A to 7 percent		<del>-</del>
2819	to a party loom 1 to the party	-1 1,536	• -
HCA	Time samuy roam, 1 to 1 percent are to 20 to 1 to 20 t	-	; _
Heo	30 to 10 percent atopesat	-1 413	_
Но	rained		·
McA	t loam, 0 to 2 percent	1,857	0.8
McB	t loam, 2 to	13	-
25.00	.lty clay loam	Ф,	
ATA	a, 0 to 2 percent	1 2 2	
Z T	silt loam	1	
1	eilt loam 6 to 15 percent		-
2 1	ailt loam 6 to 12 percent	- 13,004	
S C C	12 to 18 nercent slobe		÷ ·
NXDZ 161	HAIT LOSH 18 to 30 heroent slobes.	-1 1,223	0
MXEZ	SILL LOGHI, to CO Decrees alones a		_
MZC3	Clay loam, o to it percent alopes, actering		<u>.</u>
MzD3	clay loam, 12 to 10 percent slopes, severely		_
OcA	loam, 0 to 2 percent sl		_
OcB	loam, 2		0
Pa	silty clay loam	100 1	_
ъ	silty cl		
Pad		`	
PX	- 60	130	
A d			
RCA	iph loam, 0 to 2 percent slopes	1,421	
REB	fine sandy loam, 2 to 6 percent sic	n.	-
RAC	Rawson Variant fine sandy loam, 6 to 12 percent slopes		-
¥		25.0	-
હ	m, occasionally fl		0
E	44	1 0	-
pn	my-	0	-
No.	Whitaker loam	, יר יר	_
		-	
•		249.600	0 1 100.0
	Total		-



distribution of all the soil types subsequently mentioned with regard to the other land form - parent material associations in Huntington County.

#### Ground Moraine

The ground moraine in Huntington County is, for the part. flat and featureless, broken occasionall by stream courses and sluiceways and shallow depressions or low knolls. Soil areas are generally large relative to those in the ridge moraine due to less soil differentiation based on topographic variation in the ground moraine. The Blount and Pewamo soil series dominate (see Table 3) the landscape based on the SCS map sheets, with lesser the Patton (Pe) (See Addpendix A-1) series and only amounts of minor inclusions of the Glynwood, Rawson Variant and Haskin Vari-The latter of those series along with the Hennepin and other soil series developed primarily in areas of moraine associated with stream dissection where local relief was greater. Ground moraine occupies most of the surface area 1 n Huntington County, followed by ridge moraine.

The Blount soil series developed almost exclusively on the swells in the ground moraine of Huntington County. This series is characterized by about eight inches of a silt loam (A-4 to A-6) surface soil which is underlain to a depth of about 30 inches by a silty clay-loam (A-6 to A-7) soil (2). Beneath about thirty inches is found a clay loam (A-6 to A-7).



The Pewamo soil series is the predominant series developed in the swales and low-lying areas in the ground moraine in Huntington County. The Houghton (organic) and Patton (lacustrine) soil series also developed in some low-lying areas in the ground moraine, however, they are discussed under Depressional Deposits' and are identified with unique symbols on the engineering soils map that accompanies this report. The Pewamo soil series characterized by silty clay-loam (A-6 to A-7) soil throughout the soil profile (2). Boreholes 82, 85, 87, 92 and 93 in ground moraine swales along I-69 indicate a general soil profile consisting primarily of clay, clay loams, and silty clay-loams (A-6 to A-7). Blount and Pewamo soils, the primary constituents of the ground and ridge moraine in Huntington County, account for a combined 67.3 percent of the total county surface area (2). Ridge and ground moraine cover more than 80 percent of the county with the addition of the Morley, Haskins Variant, and other minor soil series developed on the two Wisconsinan age glacial land forms.

# Glacio-Fluvial Deposits

## Outwash Plains and Terraces

Outwash terraces are located along the Wabash River, the Little Wabash River, and the Salamonie River and on Clear Creeks and Creek in Huntington County. These deposits are composed primarily of meltwater sands and gravels and occupy somewhat higher positions in the landscape than recent river terraces (ie., from



about 25 to 50 feet above the present day flood plains). They are up to a mile in width, as is the case within the large just southeast of the Salamonie Reservoir on Salamonie River, and are found adjacent to the valley walls or on circum-navigated 'islands' in some places. The outwash plain deposits shown on the engineering soils map are all located on the floor of the old Maumee sluiceway above the flood plain (and any recent river terraces) and below the outwash terraces or the valley wall. Outwash plain deposits are composed primarily of meltwater sands and gravels and the same pedalogical soil series developed on both the plains and terraces. The outwash plains were, however, affected more by recent stream erosion and alluvial deposition due to their lower position in the landscape and proximity to the flood plain of the Little Wabash River and the Wabash River. Due to limited access and time for field sampling, some areas indicated as outwash terraces on the engineering soils are probably water-reworked till and vice-versa, as these deposits occupy similar positions in the terrain. The more level and granular areas exhibiting current marks and infiltration basins on the aerial photographs were considered outwash terraces while less level areas that had a washed or scoured appearance along the valley walls were mapped as water-reworked till. mapping discrepencies obviously must exist.

Pedological soil series that developed on the outwash plains and terraces include the Fox, Ockley, Aptakisic, and Martins-ville. These soils are generally characterized by a loam or silt



loam (A-4 to A-6) surface soil that extends to a depth of about 10 to 15 inches which is underlain to a depth of 24 to 36 inches by a loam or sandy loam (A-2 to A-6) or a gravelly-sandy loam (A-2 to A-7) subsoil (2). Beneath about 36 to 42 inches is found gravelly coarse sand (A-1 to A-3) with cobbles and boulders or a sandy loam (A-2 to A-4) with some cobbles. The Aptakisic soil developed in outwash deposited by slow moving or ponded water and occupies the low-lying positions in areas of outwash sediments. This soil is less coarse in texture than the others and is generally characterized by about nine inches of a silt loam (A-4 to A-6) surface soil which is underlain by a silty clay-loam (A-6 to A-7) subsoil to a depth of 34 inches. Beneath the subsoil is found stratified fine sandy loam (A-2) or a silty loam (A-4).

Gravel content below 36 inches is as much as 58 percent or more (2). The presence of numerous cobble and boulder-sized rock fragments in the outwash parent material was verified by roadway soil survey borehole logs.

#### Kames

No definite kames and no eskers were located in Huntington County based on comparison of the stereoscopically determined soil boundaries on the photomosaic boards with the SCS soil map sheets using the method as discussed under `GENERAL MAPPING METHOD'. The more prominent knolls in the county were identified on the soils map as possible kames regardless of the lack of certainty about them because granular material (i.e., sandy silt or



clay with some gravel) is still more likely to be found in these hill forms than elsewhere in the till plain areas. The location of these prominent, local topographic highs benefits the engineer even if they are only coarse-textured till knobs and not deposits of glacio-fluvial sand and gravel. The reader is referred to the general soil profile for outwash terraces on the engineering soils map for a general idea about the composition of these knolls identified as possible kame land forms.

#### Sluiceways

Sluiceways of both recent and meltwater origin are found in Huntington County. Those of meltwater origin are primarily located in areas of knob and basin topography, on the outwash plains and terraces, and in rugged areas of ridge moraine, while sluiceways of recent age are associated with the upper reaches of stream valleys, (ie., lower order streams), near the watershed divides. The major sluiceway systems are associated with Pony Creek in the northwest corner of the county, Loon and Majenica Creeks in the central part of the county, and Logan and Richland Creeks in the southwestern part of Huntington County.

The pedalogical soil series developed in sluiceways over till include the Pewamo and Rensselaer. The Rensselaer series is more coarse in texture and formed primarily in the larger meltwater sluiceways while the Pewamo soil developed most commonly over sluiceways of recent origin in less coarse sediments. The Pewamo soil series consists of a silty clay-loam (A-6 to A-7) with some



pebbles throughout the soil profile (2). The Rensselaer series is generally characterized by 6 to 10 inches of a loamy (A-4 to A-6) surface soil which is underlain by 10 to 14 inches of a loam (A-6 to A-7) soil and 10 to 12 inches of a clay loam (A-6 to A-7) subsoil to a depth of about 36 inches. From 36 to about 45 inches is found a loamy (A-6) soil which is underlain by a loam soil (A-2 to A-4) with lenses of sand. The Rensselaer and Martinsville soil serices are the primary soils developed in sluiceways on terraces and on outwash and lacustrine plain deposits in the Maumee Sluiceway in Huntington County. A profile for sluiceways over alluvial plains is shown on the left-hand side of the engineering soils map that accompanies this report.

# Recent Fluvial Deposits

## Flood Plains

Flood plain deposits consist of stratified alluvial sediments of recent age and are found along the Salamonie, Wabash, and Little Wabash Rivers and their major tributaries, particularly Silver, Clear, Loon, and Richland Creeks in Huntington County. The flood plains range in width from nearly half a mile in some places on the three principal rivers to a few hundred feet at points on some of their smaller tributaries. The flood plain of the Little Wabash River narrows to virtually the immediate course of the stream in the limestone area around the City of Huntington. A similar condition exists along the Wabash River near Markle and at places along the Salamonie River.



Most of the short, (ie., less than one half mile), tributary flood plains shown on the engineering soils map are not true flood plains due to steep gradients, however, they were indicated in order to show the location of these deeply eroded stream valleys or gulleys through which water frequently flows, and to maintain the continuity of the true flood plains of the major streams. Although stream action in the steep tributary valleys is primarily erosional, some alluvial sediment is, of course, deposited along these short tributaries and small alluvial fans are common where these streams empty onto the floor of the broad, flat, Maumee Sluiceway. Colluvial deposits are found on the slopes of the steep tributary valleys and, in places, at the base of the Maumee sluiceway valley walls, particularly near alluvial fans and of water-reworked till. Recent alluvium is intermixed with thin outwash over limestone bedrock and with slackwater lacustrine deposits along the Maumee sluiceway channel due to occasional flooding during periods of extreme high water. Areas beneath the Huntington and Salamonie Reservoirs were former flood plains unless otherwise indicated on the engineering soils map that accompanies this report.

Pedalogical soil series developed on flood plains in Hunt-ington County include the Eel, Genesee, Shoals and Sloan (2). These soils are generally characterized by 13 to 18 inches of a silt loam (A-4 to A-6) surface soil which is underlain to a depth of 30 to 36 inches by a loam or silt loam soil (A-4 to A-7) with thin (1/4 to 1/2 inch) layers of sandy loam (A-4). From about 36



inches to 48 inches is found a silt loam, sandy loam, or sandy silt loam (A-4 to A-6) soil which is underlain by loam or sandy clay-loam (A-4 to A-6) or gravelly-sandy loam (A-4). Gravel content ranges up to 16 percent beneath about 48 inches of overburden in areas of the Shoals soil series.

Within the river channels, limestone or dolomite bedrock is overlain by less than one foot to more than 35 feet of alluvial material in some places based on roadway soil survey boreholes data. Shallow limestone bedrock is most likely to be found beneath flood plains adjacent to areas identified on the map as "thin outwash, recent alluvium, and residual soil over limestone-dolomite bedrock" (see accompanying map). For additional information on limestone bedrock encountered beneath alluvial deposits in Huntington County, the reader is referred to Appendix B, particularly part II in the back of this report.

#### Recent River Terraces

Recent river terraces are found along the Wabash River, the Little Wabash River, and Salamonie River and their major tributaries in Huntington County. These terraces are composed primarily of stratified alluvial silt, sand, and gravel with lesser amounts of clay. They are located immediately adjacent to and about 10 to 20 feet above the flood plains and range up to about one-third of a mile in width. Recent river terrace material consists of both recently eroded sediment and reworked outwash sands and gravels. Some recent river terraces now lie beneath the high



water marks of the Huntington and Salamonie Reservoirs.

Pedalogical soil series developed on recent river terraces Huntington County are the Martinsville, Ockley, Rensselaer, i n and Whitaker (2). These series are generally characterized by a loam or silt loam (A-4 to A-6) surface soil which is underlain by clay loam (A-6 to A-7) or sandy loam (A-2 to A-6) subsoils to a depth of about 36 to 38 inches. Between about 38 and 56 inches is usually found a sandy loam (A-2 to A-4) or a gravelly sandy clay-loam (A-6 to A-7) beneath which is generally found gravelly sand (A-1) or a loamy or gravelly clay-loam (A-2 to A-4) soil with thin (< 1/2 inch) sandy lenses. Gravel content ranges up to 35 percent or more beneath about 38 inches and roadway soil survey borehole logs indicate cobbles and boulders are not uncommon in the underlying parent material of the recent river terraces, particularly in areas where limestone is at relatively shallow depth (ie., near areas indicated as thin outwash, recent alluvium, and residual soil over limestone/dolomite bedrock on the engineering soils map).

## Water-Reworked Till

Areas of water - reworked till are found throughout Huntington County adjacent to sluiceways, rivers, and streams. These deposits consist of till which was subject to sheet-wash or was commonly scoured by water during periods of seasonal flooding or after heavy rainfall, resulting in a surface soil generally more coarse in texture than the surrounding, unaffected till. Water -



reworked till is primarily a product of erosion and the resorting of existing material rather than deposition, a characteristic which seperates it from the lower-lying alluvial material and the higher ridge or ground moraine. Many of the short, steep tributaries to the old Maumee Sluiceway channel and the Salamonie River and Wabash River valleys would probably be better characterized as water - reworked till, based on the nature of the soils along these gullies. However, they were designated as flood plains on the engineering soils map for reasons already discussed in the `Flood Plains' section of this report.

Soil developed on water - reworked till in Huntington County include the Hennepin, Haskins Variant, and Rensselaer pedalogical soil series. The Hennepin soil is the most common series developed on steeply (30 to 70 percent) sloping areas of water reworked till and is characterized by a loamy (A-4 to A-7) soil throughout the profile. Some sandy layers are incorporated in the soil profile and gravel content ranges up to five percent. The Haskins Variant and Rensselaer soils are characterized by about 12 inches of a loam or sandy loam (A-2 to A-4) surface soil. The subsoil of the Rensselaer series is a loam, silt loam, or clay loam (A-6 to A-7) which is underlain at a depth of about 46 inches by a loam with sandy layers (A-2 to A-4). The subsoil of the Haskins Variant series is a loam or clay loam (A-4 to A-6) which is underlain at a depth of about 36 inches by a clay loam (A-6) with up to nine percent gravel.



Field observations made in an area of water - reworked till indicate a sandy surface soil with numerous cobbles and some boulders. Pedalogical soils developed adjacent to areas of water - reworked till includes the Martinsville and Whitaker series, and Udorthento soils developed on cut and fill areas.

## Unconsolidated Deposits Over Limestone-Dolomite Bedrock

# Thin Outwash, Recent Alluvium, and/or Residual Soil Over Limestone-Dolomite Bedrock

Thin (ie., 20 to 30 inches) glacial outwash is intermixed with recent alluvium above limestone/dolomite bedrock and any overlying residual soil along the Wabash River, the Little Wabash River, and the Salamonie River and along Rock Creek in Huntington County, Indiana. These deposits are primarily found in the form low-lying plains in the Old Maumee sluiceway channel. are also found in bench-like fashion along the Wabash River Rock Creek near the town of Markle and in a small area on the Salamonie River just southeast of Warren. Planar areas limestone/dolomite bedrock at shallow depth in the Maumee Sluiceway were not easily distinguishable from low-lying outwash and slackwater lacustrine plains, or recent river terrace deposits on the aerial photographs. Similar difficulty was encountered distinguishing terraces from limestone/dolomite benches. Liberal use was made of the SCS soil survey map sheets (2) using the color-coding system and boundary modification procedure described in the `MAPPING METHOD' section. Many of the areas determined to be underlain at a shallow depth bv



limestone/dolomite bedrock on the map sheets and aerial photographs were verified by roadway soil survey borehole data.

The Millsdale, Milton, and Randolph pedalogical soil series areas underlain at shallow depth by developed on limestone/dolomite bedrock in Huntington County, Indiana (2). Millsdale soils occupy the lower-lying positions while the Randolph and Milton series occupy intermediate and elevated positions, respectively in the landscape according to the agricultural map sheets. These soils are generally characterized by a loam or silt loam (A-4 to A-6) or silty clay-loam (A-6 to A-7) surface soil to a depth of about 7 to 15 inches. The subsoil is a clay loam (A-6 to A-7) or silty clay (A-7) which extends to limestone or dolomite bedrock at a depth of about 25 inches. Gravel or cobble-sized rock fragments are not uncommon within the soil profile and are more common on the surface than on the lacustrine plains based on limited field observations. Organic matter content ranges up to seven percent (2). Similar soils developed on the so-called klintar or limestone reefs previously discussed in the bedrock section. However, the klints are described separately as a unique land form.

## Limestone Reefs (Klintar)

Several limestone reefs, or klintar, are exposed in the Wabash sluiceway near the Wabash County line. The general nature of these limestone reefs and their likely mode of formation are discussed in detail under the bedrock section of the report and



are not here covered.

The primary pedalogical soil series developed on the reefs Huntington County is the Milton according to the SCS map sheets (2). This soil series is characterized by a silt loam (A-4 to A-6) surface soil that extends to a depth of about seven inches. The subsoil, a clay loam (A-6 to A-7) which contains residual gravel and cobble-sized rock fragments, overlies limestone/dolomite bedrock found at a depth of about 25 inches. The author investigated several of the 'klintar' on the field trip and found that the overburden thickness varied from less than half a foot to about two and one-half to three feet. The surface of the ground was uneven and not easily traversed, presumably due to solutioning effects in the underlying limestone. No true sinkholes were identified in the field, however, some small, possible sinkholes were observed on the aerial photographs. What appeared to be weakly defined concentric rings discerned on the aerial photographs on the two largest klintar in the county presumably were the surficial expression of the internal structure of the reef formations as exposed by weathering and erosion.

The reader is referred to the general soil profile of thin outwash, recent alluvium, and residual soil over limestone/dolomite bedrock for an idea of what kind of soil profile might be expected over the klintar. The klintar are, however, identified on the engineering soils map by a separate symbol as a unique land form.



# Depressional Deposits

#### Lacustrine Plain or Slackwater Plains

Lacustrine plains of both shallow lake and slackwater origin are found in Huntington County. The shallow water lacustrine plains are found in the uplands and range in size from a few acres to an area of more than one square mile as indicated in Section 26, T28N, R10E and parts of surrounding sections. The slackwater plain in Huntington County is located along the Little Wabash River in the old Maumee Sluiceway channel and is up to a mile wide in some places. One explanation of the origin of this slackwater plain is suggested under the 'Glacial Geology' section of this report. The lacustrine plains and slackwater plains are generally flat and featureless and commonly require trenches to improve sluggish drainage. No beach ridges occur on the edge of these lacustrine plains or slackwater plains.

Two different variations of the Patton soil series developed on the lacustrine plains of Huntington County; the silty Patton series developed primarily on the slackwater lacustrine plains while the more sandy Patton soil developed on both the shallow water and slackwater plains (2). The silty Patton soil is characterized by a silty clay-loam (A-6 to A-7) soil throughout its profile. The sandy Patton soil is generally characterized by about 45 to 50 inches of a silty clay-loam (A-6 to A-7) surface and subsoil which is underlain by a sandy loam or sandy clay-loam soil (A-2 to A-6). A borehole(#88 on the map) along I-69 in the



large, shallow-water lacustrine plain previously mentioned showed the following soil profile:

- 0.0' to 2.0' black clay, A-7-6(19), P.I. = 31,
- 2.0' to 4.0'; brown clay, A-6(10), P.I. = 14.

Organic matter content ranges up to six percent or more (2).

# Peat and Muck Depressions

Deposits of peat and/or muck are found in Huntington County in kettle-like, ice block, and other depressions in the glacial till and along sluiceways and in low-lying areas in stream val-The areas range in size from nearly 3/4 of a mile in leys. length and more than 60 to 70 acres to less than 5 acres. Elongate patches of peat or muck are concentrated and somewhat aligned on the edge of a band of ridge moraine south of Loon Creek in the central part of the county and in Section 11, T26N, R8E in ground moraine in the southwest part of the county. There also a concentration of depressional deposits, many of them containing peat and/or muck, in the north-central part of the county. These depressions are found primarily in the ridge moraine in the area. Elsewhere, however, there is no apparent relationship between ridge and ground moraine and the relative distribution of peat and muck.

The soil series that developed on deposits of peat and/or muck in Huntington County was the Houghton. This series is characterized by a highly organic silty clay surface soil (i.e.,



up to 15% organic matter) to a depth of about 22 inches which is underlain by peat and/or muck (A-8) (2). Organic matter content of the peat and muck ranges up to 75 percent or more. Houghton soil areas comprise less than 0.2 percent of the county surface, but knowledge of the location of these deposits is of importance to the engineer due to the high compressibility of the organic matter. Peat and muck, like glacio-fluvial lenses of sand and gravel, are incorporated in the till and can only be identified in the subsurface by drilling.

# Highly Organic Topsoil Depressions

Highly organic topsoil is found throughout Huntington County in areas ranging in size from a few acres to several of acres. Highly organic topsoil is commonly associated with or on the fringes of deposits of peat or muck and shallow or slackwater lacustrine sediments. Like deposits of peat and muck areas of highly organic topsoil are fairly well distributed throughout the county and are anomalously more numerous only in those areas described for peat and muck, particularly in the north-central part of the county.

The most common soil series containing highly organic top-soil in Huntington County included the Patton and Pewamo. The soil profile of both series is composed primarily of a silty clay-loam (A-6 to A-7), however, the Patton surface soils are underlain in many places by stratified fine sand or sandy clay-loam (A-2 to A-6) (2). Organic matter content in the surface



soil ranges from about 3 to 6 percent or more. The Millsdale and Patton (Pa) soil series are also commonly characterized by highly organic topsoils.

## Eolian Sands

Sand Dunes

Several minor, incipient sand dunes were located in Huntington County in, adjacent to, and north of the old Maumee sluiceway channel where it is occupied by the Little Wabash River. These small areas of eolian sands do not exceed about 10 to 15 feet in height and were located on the aerial photographs only after referring to the SCS map sheets and looking for the Chelsea soil series which developed on them. They are really not sand dunes at all in the classical sense, but simply isolated, randomly shaped areas where minor amounts of wind-blown sand accumulated. The most dune-like formations are located in section 14, T29N, R10E along the Little Wabash River on the floor of the Maumee sluiceway.

The Chelsea soil series developed on the deposits of eolian sand and accounts for less than 0.1 percent of the county area. This soil series is characterized by a loamy sand (A-2 to A-3) to a depth of about 54 inches which is underlain by sand (A-2-4) (2). Gravel content ranges up to 10 percent or more in the underlying material in areas where the dunes formed over fluvial deposits. Where the 'dunes' formed in ridge or ground moraine



the sandier eolian soils eventually grade in to the silty clay soils of the till. The general locations of the eolian deposits are identified on the engineering soils map by the standard crescent moon-shape used for dune deposits.

#### Miscellaneous Information

# Sand and Gravel Pits

Sand and gravel pits are found throughout Huntington County along streams and sluiceways, particularly along the Wabash River, Little Wabash River and the Salamonie River and their larger tributaries. Sand and gravel pits were not checked in the field for grain size distribution and due to the great variability of fluvial deposits, no definite determination was made as to what pits contain what size functions and what proportion. However, in general, pits located in flood plains and along shallow streams more likely produce greater amounts of sand while those in terrace and outwash plains probably produce more gravel. Some of the pits shown on the map that were identified on the 1937 aerial photographs are probably abandoned, however, they are shown on the map in order to indicate those areas where additional sand and gravel might be found. Some of the abandoned operations were partially or wholly filled with water. Numerous pits identified on the SCS soil map sheets are also shown on the map, many of which are probably still in operation.

A gravel sample taken from a pit located in an outwash terrace along the Wabash River near where Silver Creek joins it



showed the following grain size distribution:

Table 4. Grain Size Analysis of a Gravel Sample from a Pit on the Wabash River, Huntington City, Indiana (19).

Per	rcent	Size Distri	bution of Gravel	Fraction
Sand	Gravel	0.25 to 0.5 in.	0.5 to 1.0 in.	Plus 1.0 in.
5 4%	46%	28%	23%	49%

#### Quarries

Two limestone quarries were located in Huntington County as well as several abandoned operations. One is located just northwest of Bowerstown in the Old Maumee Sluiceway channel and the other is located about a mile or so southwest of the town of Markle on Rock Creek. There were several small bodies of water in the Wabash River Valley in the town of Markle and near the operation in the Maumee sluiceway that were inferred to be old quarry locations. The limestone quarried was crushed and used as aggregate for concrete, for roadstone, and as a source of agricultural lime (20).

# Cut and Fill Areas

Numerous cut and fill areas were located in Huntington County on the SCS map sheets and are shown on the engineering



soils map. They are identified by a diagonal cross-hatched pattern shown in the legend on the right-hand side of the map. No profile is given for these areas, however, they are shown on the map in order to indicate where the natural soils were distrubed.



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# Appendix A-I.ESTIMATED ENGINEERING PROPERTIES(2)

[The symbol < means less than; > means more than. Absence of an entry indicates that data were not estimated]

map symbol   Unified   AASHTO   >	ents   > 3   nches		sieve 1	number-			
	ncnes		3.0	_		Liquid   limit	Plas- ticity
	Pct	4	10	40	200	Pct	index
Aptakisic   9-34 Silty clay loam   CL, CH   A-7, A-6	0	100	100	195-100	  80-100   60-100   30-90   	25-40   35-55   20-30	5-15 20-40 NP-10
Blount   8-24 Silty clay loam,  CH, CL  A-7, A-6   0   silty clay, clay					80-95    80-95	25-40   35-60	8-20 15-35
loam.  24-60 Silty clay loam,  CL  A-6, A-7   0	0-10	90-100	90-100	80-100	70-90	20-45	10-25
	0	100		65-80    65-80			NP NP
Eel   7-13 Silt loam, loam   ML, CL   A-4, A-6	0   0   0		100	90-100  90-100  70-80		26-40   26-40   26-40	3-15 3-15 3-15
	0	95-100	85-100	75-95	  55 <b>-</b> 90	20-30	3-10
Fox     CL-ML	0-5	85-100     	70 <b>-</b> 95	50-95	  20 <b>-</b> 65   	25-45     	10-25
clay loam.  30-60 Stratified sand  SP, SM,  A-1, A-2,   0   to gravel.   GP, GM   A-3	0-10	40-100   	35-100	15-95	2-20     3-20		NP
Genesee   18-25 Silt loam, loam   ML, CL   A-4, A-6	0 İ	100	100	90=100   90=100   60=90		26-40   26-40   20-35	3-15 3-15 3-15
				80-100 75-100		23-40 l 35-55 l	4-15 15-30
	0-5	95 <b>-</b> 100	80-100	75-95	65-90	25-40	7-18
HcA   O-10 Fine sandy loam   SM, SM-SC, A-4   Haskins Variant	0 19	95-100 i	90-100	60-85	35-55	<25 i	NP-7
A-2-4,	0 19	95 <b>–</b> 100   !	90 <b>–</b> 100	50-95 i	25-75	20-30	7-12
31-60 Clay loam, silty CL A-6 0. Clay loam.	0-5	95 <b>-</b> 100  	95-100    	85-100	65-95   	30-40	10-15
the state of the s				70-100  65-100	60-95   35 <b>-</b> 95	25-40   20 <b>-</b> 50	5-20 5-25
14-60   Loam, sandy loam,   SC, SM-SC,   A-4, A-6,   O-1	0 <b>-</b> 5   8	85-100	80-100	65-100	35-95	20-50	5-25
Houghton	0						
M. 44 433 I Cooles a las institution in the contract of the co	0			80-100 i 65-90 i		22-33   20-35	\$-12 8-20
	0 j	100	90 <b>-</b> 100	60-80 j	30-60	30-40	2-8
	0   9	95-100	85 <b>-</b> 100    	80 <b>-</b> 95	40-60 i	<25     	4-9



Appendix A-I, continued

		Арр	endix A-	I, con	itinue	a						
Soil name and	Depth	USDA texture	Classif	1cation		rag- ents	P		ge pass		Liquid	Plas-
map symbol	1	1	Unified	AASHT	ro i	> 3 nches	1 4	10	1 40	1 200	limit	ticit;
	In					Pct					Pct	1 111351
Ms Millsdale	14-25   			A-6, A  A-7     		0 0-5	90-100  85-100     	80-100  80-100     	75-100  75-100       	60-95   60-95     	32-50 1 40-60	12-25 20-35
MtA, MtB, MtC M1lton		  Silt loam  Silty clay loam,   clay loam, clay.	CL	  A-4, A  A-6, A						  70-95  70-95	   26-36   32-48	4-12 12-28
	1	Clay, sandy clay   loam, channery   clay loam.  Unweathered   bedrock.		A-7, A     	-6   0	0 <b>-</b> 5	95-100	80-100   	  70-95       	  50-90       	   32-55         	14-33
MxC2, MxD2, MxE2- Morley	7-28	  Silt loam  Silty clay loam,   clay loam, clay.	CL	  A-6, A  A-6, A	-4   C	0-5   0-10	  95 <b>–</b> 100  95–100	,  95–100  90–100	  90 <b>-</b> 100  85 <b>-</b> 95	  75 <b>-</b> 95  80 <b>-</b> 90	   25-40   30-50	5-15   5-30
		Silty clay loam,   clay loam,   clay loam.		A-6, A	-7	0-10	95-100	  90 <b>-</b> 100 	  85 <b>-</b> 95 	  80 <b>-</b> 90 	   30-60 	15-30
MzC3, MzD3 Morley	4-25	Clay loam  Silty clay loam,   clay loam, clay.	CL	A-6, A		0-5   0-10	95-100 95-100	90-100	  85 <b>-</b> 95  85 <b>-</b> 95	  80-90    80 <b>-</b> 90	30-45   30-50	15-25 15-30
	25-60   	Silty clay loam, clay loam.	CL, CH	A-6, A-   	-7   C	0~10   	95-100	90-100	85 <b>-</b> 95	80-90	30-60	15-30
OcA, OcB Ockley	1 0-8 I	Loam	CL, ML, CL-ML	A−4, A⋅	-6 j	0	100	95-100	80-100	60-90	22-33	3-12
	8-40    	Fine sandy loam, clay loam, sandy loam.	CL, CL-ML,	A-6, A-2	-4	0	100	75-100	45-100	20-80	15-40	3-15
			CL, SC, aC	A-6, A-	-7   0	) <b>-</b> 2	70-85	45-75	40-70	35-55	30-50	15-30
	55 <b>–</b> 60    		SP, SP-SM, OP, GP-GM		1	-5	30-70	20 <b>–</b> 55	5-20	2-10	<b>-</b>	NP
Pa Patton		Silty clay loam		A-6 A-7		0	100			75-95   80-100		15-25 15-25
	44 <b>–</b> 60  		CL	A-6		0	100	100	95-100	75-95	25 <b>-</b> 40	10-20
Patton	18-47   47-60  	Silty clay loam   Stratified fine	CL ML, CL,	A-6  A-6, A-  A-4, A-   A-2-4   A-2-6	-7   -6,	0   0   0   1	100   100   100	100		75-100  80-100  20-80		10-20 10-25 NP-15
Pg Pewamo	12-36			A-6, A- A-7, A-					80-100  90-100		35-50   35-55	15 <b>-</b> 25 15 <b>-</b> 30
		Clay loam, silty   clay loam.	CL	A-7	0	-5	95-100	90-100	90-100	70-90	40-50	15-25
Px*, Py*.   Pits									   			

See footnote at end of table.



# Appendix A-I, continued

	r		Classif	leation	Frag-	Pe	ercentag	re nassi	ng		
Soil name and	Depth	USDA texture			lmenta			number		Liquid	Plas-
map aymbol			Unified	AASHTO	> 3  inches	4	10	40	200	limit   	ticity index
	<u>In</u>				Pct					Pct	
RcARandolph	15~25 	Loam	CL-ML, CL CL, CH	A-4, A-6   A-7, A-6		95-100   75-95 				20~38   38-74 	4-15 14-42
RgB, RgC Rawson Variant	0-10	Fine sandy loam	SM, SM-SC,	A-4	0	95-100	90-100	60-85	35-55	<25 i	NP-7
Nawson variant	10-35	Fine sandy loam, sandy loam.	SM, SM-SC,	A-4, A-2-4	i o	95-100	90-100	50-85 i	25-55	(25 i	NP-7
	35-60			A-6, A-7	0-5 	95-100	95-100	85 <b>-</b> 100	65-95	30–40   	10-16
Rk Renaselaer	0-14  14-37 	Loam	CL, ML	A-4, A-6  A-6, A-7	0 0	100 95-100	100  90-100			27-36     25-40	4-12 11-16
		Sandy clay loam,	CL, SC	A-6	0	95-100	90-100	75-95	35-75	25-35	11-16
			CL, SC, CL-ML, SM-SC	A-4, A-2	   0   	95-100	90-100	60-95	20-70	<30     	4 <b>-</b> 9
ShShoals	8-23	Silt loam  Silt loam, loam,  silty clay loam.	ICL, CL-ML	A-4, A-6	0	100 100		90-100 90-100		20-35   25-40	6-15 5-15
	23-60	Stratified silt loam to gravelly sandy loam.	ML, CL,	A-4	0-3	90-100   	85-100	60 <b>–</b> 80	50-70   	(30 )	4-10
-51.5	0-14	Silt loam		A-6, A-4	0	100	95-100	85-100	70~95	20-40	3-15
Sloan		Silty clay loam,		A-6, A-7,	0	100	90-100	85-100	75-95	30-45	8-18
		loam, silt loam.  Stratified   gravelly sandy   loam to silty   clay loam.		A-4  A-4, A-6     	0	  95-100     	70-100       	60-95     	50-90       	25-40       	3-15
Ud*. Udorthents				]   	1	 	 	 			
Wo Whitaker	0-7 7-37	Loam	CL	A-4, A-6 A-6, A-7	0		95-100  95-100			22-33 30-47	4-12   12-26
	37 <b>-</b> 60	silty clay loam,  Stratified coarae   aand to clay.		A-4	0	   98 <b>-</b> 100 	98-100 	60-85 I	40–60 	15-25	3 <b>-</b> 9
		<u> </u>	<u>'                                    </u>			<u> </u>		1	·		



# Appendix A-2. PHYSICAL AND CHEMICAL SOIL PROPERTIES (2)

[The symbol < means less than; > means more than. Entries under "Erosion factors--T" apply to the entire profile. Entries under "Wind erodibility group" and "Organic matter" apply only to the surface layer. Absence of an entry indicates that data were not available or were not estimated]

				·							
Soil name and map symbol	Depth	Clay	   Moiat   bulk	  Permeability 	  Available   water	   Soil  reaction	  Shrink-swell   potential		ors	Wind  erodi=   bility	
	<u>i</u>	i	denaity		capacity		potential	K		group	mannet
	In	Pct	0/cm3	In/hr	In/in	рН					Pct
ApAAptak1sic	1 9-34	127-35	  1.15-1.35  1.35-1.55  1.40-1.60	0.6-2.0	10.18-0.20	15.1-7.8	  Low  Moderate  Low	0.37		5	1-3
	1 8-24	135-50	1.35-1.55 1.40-1.70 1.60-1.85	0.06-0.2	0.12-0.19	14.5-7.8	Low Moderate	0.43		6 .	1-3
ChB	0-7 7-60	8-15 5-10	1.50-1.55 1.55-1.70	6.0-20 6.0-20			Low			2	.5 <b>-</b> 1
EeEel	1 7-13	18-27	1.30-1.50 1.30-1.50 1.30-1.50	0.6-2.0	0.17-0.22	6.1-8.4	Low Low	0.37		5	1-3
	1 8-30	25-35	1.35-1.55 1.55-1.65 1.30-2.20	0.6-2.0	0.15-0.19	15.6-8.4	Low Moderate Low	0.32	ì	5	1-3
	118-25	18-27	1.30-1.50 1.30-1.50 1.30-1.50	0.6-2.0	0.17-0.22	6.1-8.4	Low Low	0.371		5	1-3
	1 7-30	135-55	1.25-1.50  1.45-1.75  1.65-1.85	0.06-0.2	0.11-0.18	4.5-7.8	Low Moderate Moderate	0.321	i	6	1-3
HcAHaskins Variant	10-31	17-26	1.30-1.45 1.40-1.55 1.60-1.80	0.6-2.0	0.13-0.17	15.6-7.3	Low Low Moderate	0.32	į	3	1-3
	l 5-14	18-30	1.20-1.40 1.30-1.60 1.45-1.70	0.2-0.6	0.14-0.22	6.1-7.8	Low	0.321	1	5	1-4
Ho Houghton	0-60		0.15-0.45	0.2-6.0 (	0.35-0.45	5.6-7.8				1	>70
	8-31   31-47	18 <b>-</b> 30   10-25	1.30-1.45 1.40-1.60 1.40-1.60 1.50-1.70	0.6-2.0 0.6-2.0	0.17-0.20	5.1-6.0    5.1-6.5	Low Moderate Low Low	0.371		5     1 	1-3
		35-451	1.40-1.70		0.12-0.16	6.1-8.4	Moderate	0.321	i	6	4-7
	7-13	35 <b>-</b> 50   25 <b>-</b> 45	1.30-1.50 1.45-1.70 1.40-1.70	0.2-0.6	0.12-0.18	4.5-7.8   6.1-7.8	Low Moderate Moderate	0.371	4 1	6	1-3
MxC2, MxD2, MxE2- Morley	7-281	35-50	1.35-1.55 1.45-1.65 1.60-1.80	0.06-0.2	0.20-0.24   0.18-0.20   0.07-0.12	5.1-7.8	Low  Moderate  Moderate	0.431	3 I	6	1-3
	4-25	35-501	1.40-1.60 1.45-1.65 1.60-1.80	0.06-0.2	0.18-0.22  0.18-0.20  0.07-0.12	5.1-7.8	Moderate  Moderate  Moderate	0.431	2	7	1-3
					· ·		'				



# Appendix A-2, continued

		<del>,</del>		·		<del>,</del>					
	!	!	!							Wind	
Soil name and	Depth	Clay	Mo1st	Permeab1l1ty			Shrink-swell	fact			Organic
map symbol	!	!	bulk	ļ	water	reaction	potential	1			matter
	<u> </u>	1	density	1	capacity			K	T	group	
	In	Pet	G/cm <sup>3</sup>	<u>In/hr</u>	In/1n	рН					Pct
0.4.0-7	1 0 0	117 00	13 20 1 15	0.6-2.0	10 20 0 24	1	I Tana	10 27	-		
OcA, OcB	1 0-0	111-22	11.45-1.60	1 0.6-2.0	10.20-0.24		Low			5	-5-3
Ockley					10.15-0.20		Moderate			j .	
			1.40-1.55  1.60-1.80		10.02-0.04		Low				!
	199-00	2 <del>-</del> 5	1	1 /20	10.02-0.04	17.4-0.4	LOW	10.10			
Pa	1 0_8	127_35	1 15_1 35	0.6-2.0	0.21-0.23	6 6-7 3	Moderate	0 28	5	7	3-5
Patton			1.25-1.45		10.18-0.20		Moderate			' '	J-7
			1.30-1.50		10.18-0.22		Moderate				
	1	1	1	1 0.2-0.0	10.10-0.22		Model ave	1			
Pe	0-18	27-351	1.15-1.35	0.6-2.0	0.20-0.22	5.6-7.3	Moderate	0.28	5	7	4-6
			1.25-1.45				Moderate		ĺ	i i	
			1.20-1.501		0.06-0.141		Moderate		i	i	
	i '' ' i	o o o i	1				i	1	i	i	
Pg	0-12	27-401	1.35-1.55	0.6-2.0	0.17-0.22	6.1-7.3 I	Moderate	0.241	5 1	6 1	3-5
			1.40-1.70	0.2-0.6	0.12-0.201	5.6-7.8	Moderate	0.241	1	1	
	36-60	30-401	1.50-1.75	0.2-0.6	0.14-0.18	7.4-8.4	Moderate	0.241	- 1	ł	
	' 1	- 1	1		1	1	}	i		- 1	
Px*, Py*.		1	J		ļ	I	l l		1	i	
P1ts			Į.		l			- 1	1		
		!	!			!	_ !	!		_ !	
RcA							Low		4 1	6	1-3
		:	1.40-1.70				Moderate			}	
	25	!							1		
RgB, RgC	0 10	E 191	1 20 1 15	0.6-2.0	0 12 0 15	5672	Low	0 201	4	3	1-3
			1.40-1.551		0.13-0.15		Low		7	١	1-5
			1.60-1.80		0.13-0.15		Moderate		- 1		
	135-001	20-301	1.00-1.00	0.00-0.2	0.13-0.171	0.0-0.7	Moderate	0.311	- 1	- 1	
Rk	0_14	18_27	1 30-1 45	0.2-0.6	0.20-0.24	61_73	Low	0.28	5	5	2-6
			1.40-1.60		0.15-0.19		Moderate		7	i	2 0
			1.40-1.60		0.16-0.181		Moderate		i	i	
			1.50-1.70		0.19-0.21		Low		i		
	10000	2-301	1.50-1.70	0.0-2.0	0.13-0.211	1.9~0.4	104	0.20	i	i	
Sh	0_8	18-27	1.30-1.50	0.6-2.0	0.22-0.24	6.1-7.8	Low	0.37	5 1	5	2-5
			1.35-1.55		0.17-0.22		Low		ĺ	_ i	- /
			1.35-1.601		0.12-0.21		Low		- i	i	
		<sub>/</sub> i	1	i	i	1	i		j	1	
Sm	0-14	15-27 İ	1.20-1.40	0.6-2.0	0.20-0.241	6.1-7.8 j	Low	0.281	5 1	6 1	3-6
Sloan	14-34	22-351	1.25-1.55	0.2-0.6	0.15-0.19	6.1-8.4	Moderate	0.371	}	1	
	34-601	10-301	1.20-1.50	0.2-0.6	0.13-0.18	6.6-8.4	Low	0.371	- 1	1	
	j	- 1	1	İ		1	1	- 1		1	
Ud*.		- 1	I								
Udorthents		ļ		ł						1	
		0 !				- (			_	-	1 6
Wo							Low		5	5	1-3
			1.40-1.60				Moderate				
	37-60	3-18	1.50-1.70	0.6-2.0	0.19-0.21	6.6-8.4	Low	0.37			

Shrink-swell potential classes are based on the change in length of an unconfined clod as moisture content is increased from air-dry to field capacity. The change is based on the soil fraction less than 2 millimeters in diameter. The classes are low, a change of less than 3 percent; moderate, 3 to 6 percent; and high, more than 6 percent. Very high, greater than 9 percent, is sometimes used.



Appendix A-3. SOIL AND WATER FEATURES(2)

			Plood tog		High	water table	ble	Bedrock	ock		Risk of	corrosion
Soil name and map symbol.	Hydro-	Prequency	Duration	Months	Depth	Kind	ths	Depth	Hardness	Potential frost action	Uncoated	Concrete
	Ricap	,			띪		-	듸				
pA	υ	None			1.0-3.0	1.0-3.0 Apparent Mar-Jun	Mar-Jun	09<	1	H1gh	H1gh	Moderate.
BcB2Blount	υ	None	   	1	1.0-3.0	Perched	Jan-May	09 <		H1gh	H1gh	Moderate.
hBChelsea	∢	None		   	>6.0			09<	}	Low	Low	Low.
	υ	Occasional	Brief	Oct-Jun	3.0-6.0	Apparent	Jan-Apri	09<	1	H1gh	Moderate   	Low.
PoB, PoC2	ß	None		 ¦	>6.0			09<	1	Moderate	Low	Moderate.
Genesee	щ	Occasional	Brief	Oct-Jun	>6.0			09<	1	Moderate	Low	Low.
01ynwood	υ	None		   	2.0-3.5 Perched		Jan-Apr	09<		H1gh	H1gh	Moderate.
.ca	υ	None			1.0-2.5	Perched	Jan-Apr	09^		H1gh	High	Moderate.
HeO	Ø	None		   	>6.0			09<		Moderate	Low	Low.
Ho*Houghton	A/D	None			+1-1.0	Apparent	Sep-Jun	09<	!	H1gh	High	LOW
McA, McB	ei,	None	!	}	0.9<			09<		Moderate 	Moderate   	Moderate.
Millsdale	B/D	None		1	+1-1.0	Perched	Jan-Apr	20-40	Hard	H1gh	H18h	ro v
tA, MtB, MtC	υ	None			0.9<			20-40	Hard	Moderate	H1gh	Moderate.
MxC2, MxD2, MxE2, MxC3, MxD3	<b>ن</b>	None			>6.0			09<	ļ	Moderate	High	- Moderate.
Ockley	m 	None	 - <del>-</del>		>6.0			> 09		Moderate	Moderate	Moderate.
Patton	B/D	None			1+.5-2.0	Apparent	Mar-Jun	>60	<u> </u>	H1gh		Low.
Patton	B/D	None	 		1+.5-2.0	Apparent	Mar-Jun	>60		H1gh	- H1gh	- [Low.
					-							



# Appendix A-3 continued

			Plooding		High	water	table	Bedrock	ock		Risk of	corrosion
Soll name and map symbol	Hydro- logic	Frequency	no	Months	Depth	K1nd	Months	Depth	Hardnese	Potential   frost   action	ł	Concrete
	group				別			티				
Pg*	C/D	None			1-1-0-1-	+1-1.0 Apparent Dec-May	Dec-May	09<		t	H1gh	Low.
Exes, Pyst, Pits										1		
RcARandolph	Д	None			1.0-2.5 Perched		Jan-Apr	20-40	Hard	H1gh	H1gh	Moderate.
RgB, RgCRawson Variant	ρΩ	None		 	3.0-6.0 Perched		Jan-Apr	09^		Moderate	Low	Moderate.
Rk	B/D	None			+.5-1.0[/	+.5-1.0 Apparent Dec-May	Dec-May	09<		H1gh	H1gh	Low.
Sh	ပ	Occasional	Brief Oct-Jun 1.0-3.0 Apparent Jan-Apr	Oct-Jun	1.0-3.0	Apparent	Jan-Apr	09^		H1gh	High Low.	Low.
Sloan	B/D	Prequent Brief	Brief	Oct-Jun	0-1-0	0-1.0 Apparent Nov-Jun	Nov-Jun	09<	}	H1gh	H1gh	Low.
Udorthents Wo	ပ	None			1.0-3.0[/	1.0-3.0 Apparent Jan-Apr	Jan-Apr	09<		H1gh	H1gh	Moderate.

\* In the "High water table--Depth" column, a plus sign preceding the range in depth indicates that the water table is above the soil. The first numeral in the range indicates how high the water rises above the surface. The second numeral indicates the depth below the surface.

Flooding, the temporary inundation of an area, is caused by overflowing streams, or by runoff from adjacent slopes. Water standing for short periods after rainfall or snowmelt and water in swamps and marshes are not considered flooding.

Table 18 gives the frequency and duration of flooding and the time of year when flooding is most likely.

Frequency, duration, and probable dates of occurrence

Frequency, duration, and probable dates of occurren are estimated. Frequency is expressed as none, rare, common, occasional, and frequent. None means that flooding is not probable; rare that it is unlikely but

possible under unusual weather conditions; common that it is likely under normal conditions; occasional that it occurs on an average of once or less in 2 years; and frequent that it occurs on an average of more than once in 2 years. Duration is expressed as very brief if less than 2 days, brief if 2 to 7 days, and long if more than 7 days. Probable dates are expressed in months; November-May, for example, means that flooding can occur during the period November through May.



# Appendix A-4 CONSTRUCTION MATERIALS(2)

	White indix w	001101110011011		
Soil name and map symbol	Roadfill	Sand	Gravel	Topsoil
ApAAptakisic	Pair: wetness.	Improbable: excess fines.	  Improbable:   excess fines.	  Good. 
BcB2	Poor: low atrength.	Improbable: excess fines.	Improbable: excess fines.	Poor:   thin layer.
ChBChelsea	Good	Probable	   Improbable:   too sandy. 	Pair:   too sandy.
EeEel		excess fines.	Improbable:   excess fines. 	Good.
FoA, FoB, FoC2Fox	Good	Probable	Probable	Poor:   small stones,   area reclaim.
Ge	  Poor:   low strength.	  Improbable:   excess fines.	Improbable:   excess fines.	Good.
G1B2Glynwood	  Poor:   low strength.	  Improbable:   excess fines.	Improbable:   excess fines.	Poor:   thin layer.
HcA	Poor:   low strength.	Improbable:   excess fines.	Improbable:   excess fines.	Fair:   small stones.
HeG Hennepin	Poor: alope.	Improbable:   excess fines.	Improbable:   excess fines.	Poor:   slope.
HoHoughton	Poor:   wetness,   low strength.	Improbable:   excess humus.	Improbable:   excess humus.	Poor:   wetness,   excess humus.
McA, McB Martinsville	Good	Improbable: excess fines.	Improbable:   exceas fines.	Pair:   small stones.
Ms Millsdale	Poor:   low strength,   area reclaim,   wetness.	Improbable:   excess fines.	Improbable:   excess fines.	Poor:   wetness,   thin layer.
MtA, MtB, MtC Milton	Poor:   area reclaim,   low strength.	Improbable:   excess fines.	Improbable: excess fines.	Poor:   thin layer.
MxC2, MxD2 Morley	  Poor:   low strength.	Improbable:   excess fines.	Improbable:   excess fines.	Poor: thin layer, too clayey.
MxE2 Morley	Poor:   low strength.	Improbable:   excess fines. 	Improbable:   excess fines.	Poor:   thin layer,   slope,   too clayey.
MzC3, MzD3 Morley	  - Poor:   low strength.	  Improbable:   excess fines.	Improbable:   excess fines.	Poor:   thin layer,   too clayey.
OcA, OcBOckley	Good	- Probable	- Probable	Poor:   small stones,   area reclaim.
PaPatton	 - Poor:   low strength,   wetness.	Improbable:   excess fines.	Improbable: excess fines.	Poor: wetness.



### Appendix A-4, continued

Soil name and map symbol	Roadfill	Sand	Gravel	Topsoil
ė	  - Poor:   wetness,	    Improbable:   excess fines.	  Improbable:   excess fines.	  Poor:   wetness,
Patton	low strength.	1		too clayey.
g Pewamo	- Poor:   low strength,   wetness.	Improbable:   excess fines.	Improbable:   excess fines. 	Poor:   wetness,   too clayey. 
t <sup>a</sup> , Py <sup>a</sup> . Pits	i			
cARandol ph	  Poor:   low strength,   area reclaim.	Improbable:   excess fines.	Improbable: excess fines.	Poor:   thin layer,   too clayey.
gBRawson Variant	  - Fair:   thin layer.	Improbable:   excess fines.	Improbable:   excess fines.	Fair:   small stones.
gC Rawson Variant	- Fair:   thin layer.	Improbable: excess fines.	Improbable:   excess fines.	Fair:   small stones,   slope.
k Rensselaer	- Poor:   wetness.	  Improbable:   excess fines.	Improbable:   excess fines.	Poor:   wetness.
h Shoals	- Fair:   wetness.	Improbable: excess fines.	Improbable:   excess fines.	ÍGood∙   
mSloan	- Poor:   wetness,   low strength.	Improbable:   excess fines.	Improbable:   excess fines. 	Poor:   wetness. 
Udorthents	17.4		    Improbable:	l    Good•
Vo	- Fair:   wetness.	Improbable:   excess fines.	excess fines.	

Soils rated *good* contain significant amounts of sand or gravel or both. They have at least 5 feet of suitable material, low shrink-swell potential, few cobbles and stones, and slopes of 15 percent or less. Depth to the water table is more than 3 feet. Soils rated *fair* are more than 35 percent silt- and clay-sized particles and have a plasticity index of less than 10. They have moderate shrink-swell potential, slopes of 15 to 25 percent, or many stones. Depth to the water table is 1 to 3 feet. Soils rated *poor* have a plasticity index of more than 10, a high shrink-swell potential, many stones, or slopes of more than 25 percent. They are wet, and the depth to the water table is less than 1 foot. They may have layers of suitable material, but the material is less than 3 feet thick.



# Appendix A-5 BUILDING SITE DEVELOPMENT(2)

Soil name and map symbol	Shallow excavations	Dwellings without basements	Dwellings with basements	Small commercial buildings	Local roads and streets	Lawns and landscaping
						i
ApAAptakisic	Severe: wetness.	Severe: wetness.	Severe: wetness.	Severe: wetness.	Severe: frost action.	Moderate:   wetness.
BcB2Blount	  Sovere:   wetness.   	Severe: wetness.		Severe: wetness.	Severe: low strength, frost action.	Moderate:   wetness.
ChBChelsea	  Severe:   cutbanks cave.	S11ght=		Moderate:   slope.	Slight	  Moderate:   droughty.
Ee Eel	  Moderate:   wetness,   flooding.				Severe:   flooding,   frost action.	Moderate:   flooding. 
FoAFox	  Severe:   cutbanks cave.	  Moderate:   shrink-swell.			Moderate:   frost action,   shrink-swell.	Slight.
FoBFox	  Severe:   cutbanks cave.	  Moderate:   shrink-swell.	  Slight  	  Moderate:   shrink-swell,   slope.	  Moderate:   frost action,   shrink-swell.	Slight.
FoC2Fox	  Severe:   cutbanks cave. 		  Moderate:   slope.   	  Severe:   slope. 	Moderate:   slope,   frost action,   shrink-swell.	Moderate:   slope.
Ge	  Moderate:   flooding.	  Severe:   flooding.	  Severe:   flooding.	  Severe:   flooding.	Severe:   flooding.	Moderate:   flooding.
GlB2Glynwood	Severe:   wetness. 	  Moderate.   wetness,   shrink-swell. 	  Severe:   wetness. 	slope,	Severe:   frost action,   low strength.	Slight.
HcA Haskins Variant	  Severe:   wetness.	  Severe:   wetness.		  Severe:   wetness.	Severe:   frost action.	Moderate:   wetness.
HeG Hennepin	  Severe:   slope.	Severe:   slope.	Severe:   slope.	Severe:   slope.	Severe:   slope.	Severe:   slope.
Ho Houghton	Severe:   ponding,   excess humus.	Severe:   ponding,   low strength.	Severe:   ponding,   low strength.	Severe:   ponding,   low strength.	Severe:   ponding,   low strength,   frost action.	Severe:   excess humus,   ponding.
McA Martinsville	   Severe:   cutbanks cave. 	Moderate:   shrink-swell.	Moderate:   shrink-swell.	Moderate:   shrink-swell.	Moderate:   low strength,   frost action.	Slight.
McB Martinsville				Moderate:   shrink-swell,   slope.	Moderate:   low strength,   frost action.	Slight.
Ms Millsdale	   Severe:    depth to rock,    ponding. 	  Severe:   ponding.   	  Severe:   ponding,   depth to rock.	Severe:   ponding. 	Severe:   low strength,   ponding,   frost action.	Severe:   ponding.
MtA Milton	  - Severe:   depth to rock. 	  Moderate:   shrink-swell,   depth to rock.	  Severe:   depth to rock. 	  Moderate:   shrink-swell,   depth to rock.	  Severe:   low strength. 	
MtBMilton	Severe: depth to rock.	Moderate:   shrink-swell,   depth to rock.	Severe:   depth to rock.	Moderate:   shrink-swell,   slope,   depth to rock.	Severe:   low strength.	Moderate:   thin layer. 
		1	1			



# Appendix A-5, centinued

					<del>,</del>	
Soil name and map symbol	Shallow excavations	Dwellings without basements	Dwellings with basements	Small commercial buildings	Local roads and streets	Lawns and landscaping
MtC	Severe: depth to rock.		Severe: depth to rock.	Severe:	  Severe:   low strength.	  Moderate:   slope,   thin layer.
MxC2, MxD2 Morley	Moderate:   too clayey,   slope.	Moderate: shrink-swell, slope.	Moderate: slope, shrink-swell.	Severe:   slope.	Severe:   low strength.	Moderate:   slope. 
MxE2 Morley	Severe: slope.	Severe:   slope. 	Severe: slope.	Severe:   slope. 	Severe:   low strength,   slope.	Severe:   slope. 
MzC3, MzD3 Morley	  Moderate:   too clayey,   slope.	   Moderate:   shrink-swell,   slope.	Moderate: slope, shrink-swell.	  Severe:   slope.	Severe:   low strength.	Moderate:   slope.
Ockley	  Severe:   cutbanks cave.	  Moderate:   shrink-swell.	  Moderate:   shrink-swell.	  Moderate:   shrink-swell.	Severe:   low strength.	Slight.
OcBOckley	  Severe:   cutbanks cave. 		  Moderate:   shrink-swell.	Moderate:   shrink-swell,   slope.	Severe:   low strength.	Slight.
PaPatton	  Severe:   ponding. 	  Severe:   ponding.   	  Severe:   ponding.   	Severe:   ponding. 	Severe:   low strength,   ponding,   frost action.	Severe:   ponding.
PePatton	  Severe:   cutbanks cave,   ponding.	  Severe:   ponding.   	  Severe:   ponding.   	  Severe:   ponding.   	Severe:   low strength,   ponding,   frost action.	Severe:   ponding.
Pg Pewamo	  Severe:   ponding.   	  Severe:   ponding.   	  Severe:   ponding.   		Severe:   low strength,   ponding,   frost sction.	Severe:   ponding. 
Px*, Py*. Pits			   			
RcARandolph	Severe: depth to rock, wetness.	Severe:   wetness.	Severe:   depth to rock,   wetness.	Severe:   wetness.	Severe:   low strength,   frost action.	
RgBRawson Variant	Moderate:   wetness.	Slight	Moderate:   wetness.	Moderate:   slope.	Moderate:   frost action.	Slight.
RgCRawson Variant	Moderate:   wetness,   slope.	Moderate:   slope	Moderate:   wetness,   slope.	Severe:   slope. 	Moderate:   slope,   frost action.	Moderate:   slope. 
Rk Rensselaer	  Severe:   cutbanks cave,   ponding.	Severe:   ponding. 	Severe:   ponding.	Severe:   ponding.	Severe:   low strength,   ponding,   frost action.	Severe:   ponding. 
ShShoals	  Severe:   wetness.	Severe:   flooding,   wetness.	Severe:   flooding,   wetness.	Severe:   flooding,   wetness.	Severe:   flooding,   frost action.	Moderate:   wetness,   flooding.
SmSloan			Severe:   flooding,   wetness.	Severe:   flooding,   wetness.	Severe: low strength, wetness, flooding.	Severe:   wetness,   flooding.
Ud*. Udorthents						j 1



# Appendix A-5, continued

Soil name and map symbol	Shallow excavations	Dwellings without basements	Dwellings with basements	Small commercial buildings	Local roads and streets	Lawns and landscaping
Wo Severe: Whitaker cutban	Severe:   Severe:   cutbanks cave,   wetness	Severe:	Severe:   wetness.	Severe:   wetness.	Severe:   low strength,   frost action.	Moderate:   wetness.

limitations are considered *slight* if soil properties and site features are generally favorable for the indicated use and limitations are minor and easily overcome; *moderate* if soil properties or site features are not favorable for the indicated use and special planning, design, or maintenance is needed to overcome or minimize the limitations; and *severe* if soil properties or site features are so unfavorable or so difficult to overcome that special design, significant increases in construction costs, and possibly increased maintenance are required. Special feasibility studies may be required where the soil limitations are severe.



Appendix A-6 SANITARY FACILITIES(2)

and "	Appendix	A-6 SANITA	RY FACILITIES	(4)	
Soil name and map symbol	Septic tank absorption fields	Sewage lagoon areas	Trench sanitary landfill	Area anitary landfill	Daily cover for landfill
ApAAptakiaic	Severe: wetness.	Severe: wetness.	  Severe:   wetness.	Severe:   wetness.	Poor: wetness.
BcB2 Blount	Severe:   wetness,     percs slowly.	Severe: wetness.	Severe:   wetness.	Severe:   wetness.	Poor: wetness.
ChBChelsea	  Severe:	Severe: seepage.	Severe:   seepage,   too sandy.	Severe:   seepage.	Poor: too sandy, seepage.
Eel	  Severe:	Severe: flooding, wetness.	  Severe:   flooding,   wetnesa.	Severe:   flooding,   wetness.	Pair: too clayey, wetness.
FoA, FoBFox	Severe:   poor filter.	Severe: seepage.	  Severe:   seepage,   too sandy.		Poor: aeepage, too sandy, small atones.
FoC2	  Severe:   poor filter.	Severe: seepage, slope.		  Severe:   seepage. 	Poor:   seepsge,   too sandy,   small stones.
Ge	  Severe:   flooding.	Severe:  flooding.	  Severe:   flooding.	  Severe:   flooding.	  Good. 
GlB2Glynwood	  Severe:   percs slowly,   wetness.	  Moderate:   slope. 	Moderate:   wetness,   too clayey.	Moderate:   wetness.	Fair:   too clayey,   wetness.
HcAHaskins Variant	i	  Severe:   wetness.	  Severe:   wetness.		  Poor:   wetness.
HeG Hennepin	  Severe:   percs slowly,   alope.	  Severe:   slope. 	  Severe:   slope.		  Poor:   slope. 
Ho Houghton	1	  Severe:   seepage,   ponding,   excess humus.		Severe:   ponding,   seepage.	Poor:   ponding,   excess humus.
McA Martinaville	   Slight  	  Moderate:   seepage. 	  Moderate:   too clayey. 	Slight	Fair:   too clayey,   thin layer.
McB Martinsville	    Slight  	  Moderate:   seepage,   slope.	  Moderate:   too clayey.	Slight	Pair:   too clayey,   thin layer.
Ms Millsdale	  - Severe:   depth to rock,   ponding,   percs slowly.		  Severe:   depth to rock,   ponding,   too clayey.	Severe:   depth to rock,   ponding.	Poor:   too clayey,   area reclaim,   hard to pack.
MtA, MtB	  Severe:   depth to rock,   percs slowly.	Severe:   depth to rock. 	Severe:   depth to rock,   too clayey.	Severe:   depth to rock.	Poor:   area reclaim,   too clayey,   hard to pack.
MtC	-  Severe:   depth to rock,   percs slowly.	  Severe:   depth to rock,   slope.	  Severe:   depth to rock,   too clayey.		Poor:   area reclaim,   too clayey,   hard to pack.
MxC2, MxD2 Morley	- Severe:   perco slowly.		  Moderate:   slope,   too clayey.	Moderate:   slope.	Pair: too clayey, slope.
MxE2 Morley	  - Severe:   percs slowly,   slope.	  Severe:   slope.	  Severe:   slope.		Poor:
MzC3, MzD3 Morley	Severe:   percs slowly.	Severe:   slope.	Moderate:   slope,   too clayey.	Moderate:   slope.	Fair:   too clayey,   slope.



### Appendix A-6, continued

		T		1	T
Soil name and map symbol	Septic tank absorption fields	Sewage lagoon areas	Trench sanitary landfill	Area sanitary landfill	Daily cover for landfill
OcA, OcB Ockley	Slight	- Severe:   seepage.			Poor:   small stones.
PaPatton	Severe:   ponding,   percs slowly.	Severe:   ponding.	Severe:   ponding.	Severe:   ponding.	Poor:   ponding.
PePatton	Severe:   ponding,   percs slowly.	Severe:   ponding.	Severe:   ponding.	Severe:   ponding.	Poor:   ponding.
Pg Pewamo	Severe:   percs slowly,   ponding.	Severe:   ponding.	Severe:   ponding,   too clayey.	Severe: ponding.	Poor:   too clayey,   ponding,   hard to pack.
Px#, Py#. Pits					1
RcARandolph	Severe:   depth to rock,   wetness,   percs slowly.	Severe:   depth to rock,   wetness.	Severe:   depth to rock,   wetness,   too clayey.	Severe:   wetness,   depth to rock.	Poor:   too clayey,   area reclaim,   hard to pack.
RgBRawson Variant	Severe:   wetness,   percs slowly.	Severe:   wetness.	Moderate:   wetness.	Slight	Fair:   wetness.
RgC Rawson Variant		Severe:   slope,   wetness.	Moderate:   wetness,   slope.	Moderate:   slope.	Fair:   slope,   wetness.
Rk	Severe:   ponding.	Severe:   ponding.	Severe: ponding, too sandy.	Severe:   ponding.	Poor:   too sandy,   ponding.
ShShoals	   Severe:   flooding,   wetness.	Severe:   flooding,   wetness.	Severe:   flooding,   wetness.	Severe:   flooding,   wetness.	Poor:   wetness.
SmSloan	Severe: flooding, wetness, percs slowly.	Severe:   flooding,   wetness.	Severe:   flooding,   wetness.	Severe:   flooding,   wetness.	Poor:   wetness. 
Ud*. Udorthents		:			
Wo Whitaker	Severe:   wetness.	Severe:   wetness.	Severe:   wetness.		  Poor:   wetness.

The limitations are considered *slight* if soil properties and site features are generally favorable for the indicated use and limitations are minor and easily overcome; *moderate* if soil properties or site features are not favorable for the indicated use and special planning, design, or maintenance is needed to overcome or minimize the limitations; and *severe* if soil properties or site features are so unfavorable or so difficult to overcome that special design, significant increases in construction costs, and possibly increased maintenance are required.

Table 13 also shows the suitability of the soils for use as daily cover for landfills. A rating of *good* indicates that soil properties and site features are favorable for the use

and good performance and low maintenance can be expected; fair indicates that soil properties and site features are moderately favorable for the use and one or more soil properties or site features make the soil less desirable than the soils rated good; and poor indicates that one or more soil properties or site features are unfavorable for the use and overcoming the unfavorable properties requires special design, extra maintenance, or costly alteration.



## Appendix A-7 WATER MANAGEMENT

		imitations for-		Pe	atures affecting	
Soil name and map symbol	Pond reservoir areas	Embankments, dikes, and levees	Aquifer-fed excavated ponds	Drainage	Terraces and diversions	Oranged waterways
ApAAptakiaic	Moderate:	Severe: piping, wetness.	  Moderate:   alow refill. 	Frost action	Erodes easily, wetness.	Wetness, erodes easily.
BcB2Blount	Moderate:	Moderate: piping, wetness.	  Severe:   no water. 	Percs slowly,   frost action,   slope.	Erodes easily, wetness, percs slowly.	Wetness, erodes easily.
ChBChelsea	Severe:   aeepage.	Severe: piping, seepsge.	  Severe:   no water. 	  Deep to water   	Too sandy, soil blowing.	Droughty.
Ee	Moderate:	Severe: piping.	  Moderate:   deep to water,   slow refill.	  Deep to water   	  Erodes easily   	Erodes easily.
FoA, FoBFox	Severe:     seepage.	Severe: seepage, piping.	  Severe:   no water.	  Deep to water   	  Too sandy  	Rooting depth.
FoC2Fox	  Severe:	Severe: seepage, piping.	  Severe:   no water. 	  Deep to water 	  Slope,   too sandy.	Slope, rooting depth.
Ge	· 1	Moderate: piping.	  Severe:   no water.	  Deep to water 	Erodes easily	Erodes easily.
Q1B2	  Moderate:	Moderate: wetness, piping.	  Severe:   no water.	Slope,   percs slowly,   frost action.	Erodes essily, wetness, percs slowly.	Erodes easily, percs slowly.
HcAHaskina Variant	  Moderate:   seepage. 	Moderate: piping, wetness.	  Severe:   no water.	Perca slowly,   frost action.	Wetness, soil blowing, percs slowly.	Wetness,   percs slowly.
HeQ Hennepin	  Severe:   slope.	Severe: piping.	  Severe:   no water.	Deep to water	Slope,   percs slowly.	Slope,   droughty,   percs slowly.
Ho Houghton	  Severe:   aeepage.	Severe: excess humus, ponding.	  Severe:   alow refill.	  Frost action,   subsides,   ponding.	Ponding,   soil blowing.	  Wetness. 
McA	  Moderate:   seepage.	Severe: thin layer,	  Severe:   no water.	  Deep to water   	Erodes easily	Erodes easily.
McB	  Moderate:   aeepage,   slope.	  Severe:   thin layer,   piping.	  Severe:   no water.	  Deep to water 	Erodes easily	Erodes easily.
Ma Millsdale	1	  Severe:	  Severe:   no water.	  Depth to rock,   frost action,   ponding.	Depth to rock, ponding.	Wetness, depth to rock.
MtA	  Moderate:   depth to rock.	  Severe:   thin layer.	Severe:   no water.	Deep to water	1	depth to rock.
MtB	  Moderate:   depth to rock.   slope.	  Severe:   thin layer. 	Severe: no water.	Deep to water	Depth to rock, erodes easily.	Erodes easily, depth to rock.
MtC Milton		  Severe:   thin layer.	Severe:   no water.	Deep to water	Slope,   depth to rock,   erodes easily.	Slope,   erodes easily,   depth to rock.



### Appendix A-7, continued

	1.	imitations for		Pe	atures affecting	
Soil name and map symbol	Pond reservoir	Embankments, dikes, and	Aquifer-fed excavated	Drainage	Terraces and	Grassed
map symbol	areas	levees	ponds		diversions	waterwaya
MxC2, MxD2, MxE2, MzC3, MzD3 Morley	Severe: alope.	Slight	Severe: no water.	Deep to water	Slope, erodes easily, percs slowly.	Slope, erodes easily, percs slowly.
OcAOckley	Moderate: seepage.	11040144	Severe: no water.	Deep to water		Erodes easily.
	Moderate:   seepage,   slope.	11000.00.	Severe: no water.	Deep to water		Erodes easily.   
Pa	Slight	Severe: ponding.		Ponding, frost action.	Ponding	Wetness     
PePatton	Slight	Severe: ponding.		Ponding, frost action.	Erodes essily, ponding.	Wetness,   erodes easily. 
Pg Pewamo	  S11ght  	Severe:   ponding.	  Severe:   slow refill. 	  Ponding,   frost action.	Ponding	Wetness.
Px#, Py#. Pits				[   	! 	! 
RcARandolph	Moderate:   depth to rock.	1001010	Severe:   no water. 	Depth to rock,   frost action.	Depth to rock,   wetness,   erodes easily.	Wetness,   depth to rock,   erodes easily.
RgBRawson Variant	  Moderate:   seepage,   slope.	Severe:   piping.	Severe:   no water.	Deep to water	Erodes easily,   soil blowing. 	Erodes essily,   percs slowly.
RgCRawson Variant	  Severe:   alope.	Severe:   piping.	Severe: no water.	Deep to water	Slope,   erodes easily,   aoil blowing.	Slope,   erodes easily,   percs slowly.
Rk	  Moderate:   aeepage.	Severe:   piping,   ponding.	Severe:   cutbanks cave.	Ponding,   frost action,   cutbanks cave.	Ponding,   too sandy.	Wetness.
ShShoals	  Moderate:   seepage.	Severe:   wetness,   piping.	Moderate:   slow refill.	Flooding,   frost action.	Erodes easily, wetness.	Wetness,   erodes easily.
SmSloan	  S11ght	  Severe:   piping,   wetness.	Severe:   slow refill.	Flooding,   frost action.	Erodes easily, wetness.	Wetness,   erodes easily.
Ud*. Udorthents						
Wo Whitaker	   Moderate:   seepage.	Severe:   wetness.	Moderate:   slow refill,   cutbanks cave.	cutbanks cave.	Erodes easily, wetness.	Wetness,   erodes easily.

The limitations are considered *slight* if soil properties and site features are generally favorable for the indicated use and limitations are minor and are easily overcome; *moderate* if soil properties or site features are not favorable for the indicated use and special planning, design, or maintenance is needed to overcome or minimize the limitations; and *severe* if soil properties or site features are so unfavorable or so difficult to overcome that special design, significant increase in construction costs, and possibly increased maintenance are required.



# Appendix A-8 RECREATIONAL DEVELOPMENT(2)

Ner	rippoliuli ri	O NEONEA NO			
Soil name and map symbol	Camp areas 	Picnic areas	Playgrounds	Paths and trails	Golf fairways
ApAAptakisic	Severe:   wetness.	Moderate: wetness.	Severe: wetness.	Moderate:	Moderate:   wetness.
BcB2Blount	  Severe:   wetness. 		Severe: wetness.	Moderate:   wetness.	Moderate:   wetness.
ChBChelsea	  Slight	  Slight	   Moderate:   slope.	  Slight  	  Moderate:   droughty.
EeEel	Severe:   flooding.	Slight	Moderate: flooding.		Moderate:   flooding.
FoAFox	Slight	Slight	Moderate:   small stones.	Slight	Slignt.   
FoBFox	Slight	Sl1ght	Moderate:   slope,   small stones.	Slight	Slight.
FoC2Fox	  Moderate:   slope.	,	  Severe:   slope.	  Slight  	  Moderate:   slope. 
Ge	Severe:   flooding.	Slight	Moderate:   flooding.	Slight	Moderate:   flooding.
GlB2Glynwood			   Moderate:   wetness,   slope,   percs slowly.		Slight.     
HcA Haskins Variant	  Severe:   wetness.	  Moderate:   wetness,   percs slowly.	  Severe:   wetness. 	  Moderate:   wetness. 	  Moderate:   wetness. 
HeG		Severe:   slope.	Severe:   slope.	Severe:   slope.	Severe:   slope.
HoHoughton	Severe:   ponding,   excess humus.	Severe:   ponding,   excess humus.	Severe:   ponding,   excess humus.	Severe:   ponding,   excess humus.	Severe:   excess humus,   ponding.
McA Martinsville	Slight	Slight	Slight	Slight	Slight.
McB Martinsville	Slight	Slight	Moderate:   slope.	Slight	Slight.
Ms Millsdale	Severe:   ponding.	Severe:   ponding.	Severe:   ponding.	Severe:   ponding.	Severe:   ponding.
MtA	- Moderate:   percs slowly.	Moderate:   percs slowly.	Moderate:   percs slowly.	Slight	thin layer.
MtBMilton	- Moderate:   percs slowly.	Moderate:   percs slowly.	Moderate:   slope,   depth to rock,   percs slowly.		thin layer.
MtC Milton	Moderate:   slope,   percs slowly.	Moderate:   slope,   percs slowly.	Severe:   slope.	Slight	slope,   thin layer. 
MxC2, MxD2 Morley	Moderate:   slope,   percs slowly.	Moderate:   slope,   percs slowly.	Severe:   slope. 	Severe:   erodes easily.	Moderate.   slope. 



## Appendix A-8, continued

Soil name and map symbol	Camp areas	Picnic areas	Playgrounds	Paths and trails	Golf fairways
	İ				
MxE2 Morley	Severe:   slope.	Severe: alope.	Severe:	Severe: erodes easily.	Severe:   slope. 
MzC3, MzD3 Morley	Moderate:   slope,   percs slowly.	Moderate: alope, percs slowly.	Severe:   slope.	Severe: erodea easily.	Moderate:   slope. 
Ockley	Slight	Slight	Slight	Slight	Slight.
OcBOckley	Slight	Slight	Moderate:	Slight	Slight.
PaPatton	Severe:   ponding.	Severe: ponding.	Severe:     ponding.	Severe:   ponding. 	Severe:   ponding.
PePatton	Severe:   ponding.	Severe: ponding.	Severe:     ponding.	Severe:   ponding.	Severe:   ponding. 
PgPewamo	Severe:   ponding.	Severe: ponding.	Severe:   ponding.	Severe:   ponding. 	Severe:   ponding.
Px*, Py*. Pits					
RcA Randol ph	Severe:   wetness.	Moderate:   wetness,   percs slowly.	Severe:   wetness.	Moderate:   wetness. 	Moderate:   wetness,   thin layer.
RgBRawson Variant	  Moderate:   percs slowly. 	Moderate:   percs slowly.	Moderate:   slope,   percs slowly.	Slight	Slight.
RgCRawson Variant	  Moderate:   alope,   perca slowly.	Moderate: alope, percs slowly.	Severe:   slope. 	Slight	Moderate:   slope.
Rk Rensselser	  Severe:   ponding.	  Severe:   ponding. 	Severe:   ponding.	Severe:   ponding. 	Severe:   ponding.
ShShoals	Severe:   flooding,   wetness.	Moderate:   wetness.	Severe:   wetness.	Moderate:   wetness.	Moderate:   wetness,   flooding.
SmSloan	Severe:   flooding,   wetness.	Severe:   wetness.	   Severe:   wetness,   flooding.	Severe:   wetness. 	Severe:   wetness,   flooding.
Ud*. Udorthenta			8		
WoWhitaker	Severe:   wetness.	Moderate:   wetness.	Severe:   wetness.	Moderate:   wetness.	Moderate:   wetness.

properties are generally favorable and that limitations are

Slight means that soil

minor and easily overcome. *Moderate* means that limitations can be overcome or alleviated by planning, design, or special maintenance. *Severe* means that soil properties are unfavorable and that limitations can be offset only by costly soil reclamation, special design, intensive maintenance, limited use, or by a combination intensive maintenance, limited use, or by a combination

of these measures.



APPENDIX B Part I

Roadway Soil Borehole Data

		6 19 21 21 - 128.8 8 NP 11 NP 22 8		
PI			152	18.0 7 17 7 17 18.0
PL		15 18 (pct) 18 13 NP 18 NP 13 10 NP	777	118
LL		21 37 Dens. 39 Dens. 21 NP 42 42 42 12 NP 42	25 42	Moist. 29 22 34 Moist.
ပ		7 37 18 18 3 4 4 26 10 18 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	35	
Percent S M		14 33 Max. 41 Max. 18 49 66 21 50 18 18	31 35	- 125.1; Opt. 58
Pe <sub>1</sub>		-79- -30- 11.6; 1 -41- 15.8; 1 -79- -69- -79- -79- -79-	1	
on AASHTO		A-1-b(0) A-6(11) moist ] A-6(9) Moist ] A-6(2) A-4(4) A-2-4(0) A-2-4(0) A-2-4(0) A-1-b(0) A-1-b(0)	A-6(7) A-7-6(12)	Wet Dens. A-6(2) A-4(8) A-6(7) Wet Dens.
Classification Textural AA	608(2), SR 221	Br. Sndy. Lm Br. Clay  ty (pct) - 122.5; Opt. Br. Loam ty (pct) - 110.9; Opt. Br. Sndy. Lm. Br. Loam Gray Slty. Cl. Lm. Br. Sndy. Lm. Br. Lm. w/tr Organic Br. Lm. w/tr r. organic Br. Lm. w/tr. organic Br. Lm. w/tr. Br. Sndy. Lm. Br. Sndy. Lm.	85(b), S.R. 124  Gray Clay Br. Cl. Lm. organic	y (pcf) - 105.7; Max. Br. Sandy Loam Br. Silty Loam Br. Clay w/tr y (pct) - 115.5; Max.
Sample Depth(ft.)	S-Project No.	4.0- 6.0 4.0-10.0 Dry Density 0.5-10.0 Dry Density 2.0- 4.0 6.0- 7.5 11.0-12.5 5.0- 6.5 5.0- 6.5 2.0- 4.0 0rg 8.0-10.0 w/tr. 4.0- 6.0	S-Project No. 8.0-10.0 c. 0.5-2.0 w/tr.	Dry Density 2.0- 3.0 0.5- 2.0 0.5- 6.5 Dry Density
Offset	S	10'Lt.  b b c b c b c c l c l c l c l c l c l	S-F 15'Lt.	35'Lt. 25'Rt. 15'Lt.
Sample Station		906+00 917+00 939+60 951+20 951+20 956+00 961+70 970+00	1191+00	1199+55 1231+60 1239+00
Job borehole#		1 3 6 7 9 9 10 11 11	1 -	2 2 2
Map Sorettie #		m 171 10 10 10 10 10 10 10 10 10 10 10 10 10	16.3	12.2



PART I - Continued

																15.8				18.0							(	(1,
ſ																; Opt. moist.				moist.		1						Wet Dens(per)
PI	29	17	MP	00	22	6	18	2	21		2	11	25		26	t. II	12		23		25				20	36	77 .	vet.
PJ	26	15	NP	16	20	15	18	13	18		15	17	23		18	; Op	18		17	1; Opt.	19				91	200		Max.
LL	55	32	MP	24	42	24	36	18	39		20	28	48		77	- 126.2	30		70	-125.					36	89		17.S; M
Percent G S M C	-21- 63 16	-67- 20 13	-73- 18 9	27	-36- 28 36		58		52		-35- 52 13	-70- 17 13	-18- 41 41		32- 25 43	Wet Dew.	48- 25 27		-56- 11 33	Wet Dens.	39- 22 39				32		16	1
ASHTO	A-7-6(19)	A-2-6(1)	A-2-4(0) -		(1)			_			A-4(7)	(0	~		A-7-6(14) -32- 25	. 108.6; Max. Wet Dew.	A-6(4)		A-6(9)	105.7; Max. Wet Dens.	A-7-6 (12)-39-					0	A-6(10) -	108.2; Opt. Moist.
ple Classification th(ft.) Textural A	Gr. Slty. Lm.	W/trace organic Gr. Sandy loam	W. crace organic Br. Sandy loam	Br. Sandy loam	Br.e Gray Clay	Brown Sandy	Gray Silty Loam	Gray Sandy Loam	Br. Slty. Cl. 1m.	w/trace organic	Br. Silty Loam	Br. Sandy Loam	Tan Clay w/trace	Organic	Tan Clay	Dry Density (pcf) -	Mottled Gr.e Br.		Brown Sandy Clay	Dry Density (pcf) -	Brown Clay		S.R. 9 and 37		Brown Clay	Br. Slty. Cl. Lm.	Lt. br. Sulty. Lm.	Dry Density (pcf) - -127 6
Sample Depth(ft.)	3.0- 4.0	9.0-10.0	15.0-16.0	3.0- 4.0	3.0- 4.0	1.0- 2.0	14.0-15.0	20.0-21.0	1.0- 2.0		10.0-11.0	10.0-11.0	1.0- 2.0		0.2- 6.0		2.5- 3.5		0.5-3.0		1.0 - 3.0		t F-101 (8),		1.0-2.0	2.0	2.0	
Offset	65'Rt.	65'Rt.				্ব		ā	'n		Ţ	ŭ	Ţ		ū		10'R		ч		10'R		Project		20'Ft.	37'J.t.	29'Rt.	
Sample Station	1243+50	1243+50	1243+50	1249+90	1267+20	1305+75	1305+75	1305+75	1316+10		1328+00	1361+00	1373+00		1389+00		1398+50	() () ()	1430+00		1460+00				628+00	635+85	643+00	
Map borehole #	6	6	6	10	11	17	17	17	18		20	25	28	,	31		33	Ç	39		42			,	→ (	7	m	
Map borehole #	14	14a	14b	15	16	1,7	17a	17b	. 18		19	20	21	Č	2.2	1	23	ò	47	(	25				97	17	87	



PART I - Continued

			9.	- :	78 -											~						
PI	25	37	14 24 27 (pct)-127.6	23	15		11	77	7 t	10	15	CT	n 0		NP 21	wet dens.(pct)-124.8	16	91		7 T	2 5	0.7
PL	22	38	737	24	22		16	10	16	2 0	17	) T	119		NP	s. (pc	1.6	17		91	20 0	2
LL	47	75	9 16 31 1 12 27 47 2 13 31 54 2 Max. Wet Dens.	47	37		27	, r	77	7 7	200	7 7	28		NP 46	t den	2.3	33		30	100	) ?
O	21	22	16 27 31 × We	26	15		47	17	200	2 7 7	10	7 4	1		27		25	22		40	5 0	7· ~
Percent S M	62	89	מעטע)	54	27		10	ינ	3 6	ι α	2 2	7 -	1		77	; Max.	6.7	55	1	n :	04	-
Per G S	- 17 -	- 10 -	-55- -21- -16- t17.8;	- 20 -	- 58 -		- 43 -	- 28 -	07	3,7		ά	82		- 92 - - 29 -	0.	- 32 -	23			- 747 -	
ion AASHTO	A-7-6(14)	A-7-5(20)	A-6(4) - 55- A-7-6(15) - 21- A-7-6(18) - 16- Opt. Moist17.	A-7-6(15)	A-6(3)		A-6(5)	A-6(9)	A-7-6(14)	A-6(8)	A-6(8)	A-2-4(0)	A-2-4(0)		A-1-a(0) A-7-6(13)		A-6(0)	A-6(10)		A-6(10)	A = 2 - 64 / 2	(+)0-7-0
Classification Textural AA	Gray Slty. Cl. Lm. w/some Marl & trace	organic Bl. Slty. Cl. Lm.	W/trace organic Gray Sandy Loam Br. Silty Clay Lm. Br. Silty Clay Dry Density(pct)-108.2;	Lt. Br. Slty. Cl.	Loam Dk. Br. Sndy. Loam w/trace organic		Brown Clay	Br. Silty Loam					Dk. Br. Sand 2/trace organic		Lt. Br. Clay Lm.	Dry Density(pct)-104.2;	Brown Clay Loam			Broup loam	Mottled Br & R1	5
Sample Depth(ft.)	5.0- 6.0	0.8- 2.5	6.0- 7.0 1.0- 7.0 1.0- 5.0	0.5-7.0	3.0- 4.0		6.0-8.0	0.0 - 1.0	3.0- 4.0	1.5 - 2.5	2.0- 4.0	14.0-16.0	2.0- 4.0	0 71 0 61	1.0- 2.0		6.0- 7.0	2	7 0 8 0	- 0	- ac	;
Offset	ង	37'Rt.	37'Rt. 37'Rt. 37'Rt.	37'Rt.	37'Rt.		40'Lt.	37'Lt.	37'Lt.	37'Rt.	37'Rt.	37'Rt.	37'Rt.	37 t D+	37'Rt.		80'Lt.	37'Lt.	3711	165 Lt.	165'Lt.	
Sample Station	662+00	683+50	683+50 702+50 710+00	725+00	734+65		750+00	774+00	785+00	817+00	833+80	833+80	845+75	87,5475	870+60		891+50	0 #906	00+906	912+00	912+00	
Job Borehole #	٢	12	12 13(10w) 14	16(high)	18		22	25	28	32	35	35	38	38	42		46(h1gh)	48	48	51	51	
Map Borehole #	29	30	30a 31 32	33	34	4	35	36	37	38	39	39a	40	403	41		42	43	43a	44	440	



PART I - Continued

PI	NP 18		12	14	35		7		_			20			39	13			10	1		7	
PL	NP 22		19	18	39	16	21	21	17	19	16	20	21	(	23	38	22	1	7.7	1		1/	
II	NP 40		31	32	74	27	41	29	31	23	28	70	35	(	7.9	51	31	(	32			21	
C	14		42	48	12	31	11	33	33	∞	24	23	17		33	14	21		12		ı	2	
Percent S M	26		53	77	14	40	16	23	04	85	34	94	61		48	61	61		34		1	30	
Per G S	-95-		- 5-	8 -	-74-	-56-	-73-	-44-	-27-	- 7-	-42-	-31-	-22-		-19-	-25-	-18-		-24-	1	1	-69-	
tion AASHTO	A-1-6(0) A-6(11)	1 9 Bypass	A-6(9)	A-6(10)			A-2-7(1)	A-4(5)	A-6(10)		A-6(6)	A-6(11)	A-6(10)		A-7-6(20)	A-7-5(11)	n A-4(8)		. A-4(3)	A-4 to	A-6	A-4(0)	
Classification Textural	Brown Sand Brown Silty Loam	. 888(3), S.R. 37 and	Mott. Gr. & Yellow Silty Clay	Gray Clay	Lm. w/ little Organ	Gray Clay	Br. Sandy Loam	Yellow Clay	Lt. Br. Clay	Mott-yelGray/silt	Br. Clay Loam	Dk. Br. Clay Loam	Lt. Br. Silty Loam	4.5'	Brown Clay 5.5'	Bl. Silty Loam	Yel. Silty Cl. Loam A-4(8)	7.5	Reddish Br. Sndy. Jm. A-4(3) 6.0'	Alluvium to	a.m.s.l. bedrock	Br. Sandy Loam	.0
Sample Depth(ft.)	14.0-15.0 0.0- 1.0	F-Project No.	3.5- 6.5	6.5-11.0		11.5-13.0	6.5-8.0	0.5- 4.0	8.0-15.5	11.5-14.0	10.5-15.0	2.5- 6.0	4.0- 4.5	refusal @ 4		0.	2		0.0- 5.0 refusal@6		-	4.0- 6.0	1
Offset	165'Lt. 37'Rt.	Ħ	15'Lt.	15'Lt.	יאן רד		37'Rt.					37'Rt.	37'Rt.		20'Lt.	37'Rt.	37'Rt.		20'Lt.	25'Rt.		20'Rt.	
Sample Station	912+00		118+00	118+00	777	130+00	136+00	142+00	166+00	172+00	181+00	193+00	199+00		211+00	232+00	232+00		252+50	256+11		200+80	(new tine)
Map borehole #	51		7	4 u	<b>1</b>	8	10	12	20	22	25	29	31		35	42	42		64	B-5		52	5
Map borehole #	44b 45		97	46a	ì	48	67	50	51	52	53	54	55		56	57	57a		58	59		09	



PART I - Continued

	1								
	PI		NP	9		NP	2		4
ļ	PL		NP			NP	14		23
	ΓΓ		NP	23		NP	16		8 54 38 27 23
	υ		22	32		12	54		38
Percent	M		18	16		⊣	16		54
Per	S		-60- 18 22 NP	-52-		87 1	09		∞
ι	AASHTO G S M C LL PL PI		A-4(1)			A-1-b(0)	A-4(1)		A-4(8)
Classification	Textural	F-Project No. 888(1), S.R. 37 Bypass	Sndy Cl. Loam	Sndy Clay	.0.	Sand some gravel	Sndy. Cl. Im w/	little gravel	Silty Clay
	Depth(ft.)	ject No. 88	0.0- 2.0	2.0- 4.0	refusal @ 8.0	37'Rt. 38.0-40.0	37'Rt. 2.5- 4.0		37'Rt. 0.0- 1.0
	Offset	F-Pro	37'Rt.	37'Rt.		37'Rt.	37'Rt.		
	Station		204+00	204+00		216+00	221+00		240+00
	Borehole #		MZ002	MZ002		MZ011	MZ013		MZ200
	Borehole # Borehole # Station Offset Depth(ft.)		61	61a	ę	62	63		<b>79</b>

PART I - Continued

										L -																			
PI	12 13 20	10	7 01	11	6	11	15	12	20	6	NP	11		0	1 5	18			11	12	14	22	11	2	19.	5	~7	36	
PL	17 59 27	15	22	15	15	39	23	16	61	16	NP	15		14	16	13			16	13	82	8 2	13	25	16	25	12	52	7
TT	29 72 47	25	29	26 26	24	20	38	28	81	25	NP	26		16	3.	31			27										
ပ	50 26 57	65	ŀ									34																	
Σ	25 22 42	27	37	28	21	37	43	19	30	21	7	14		7	12	0													
S 5	- 25 - - 52 - - 1 -	- 24 -			- 30 -		- 4-					- 52 -			37	62			30	14	23	22	31	55	32	17	26	16	
AASHTO	A-6(9)  A-4(8)	A-4(8)	A-4(8) A-6(11)	A-6(8)	A-4(7)		A-6(10)	A-6(8)	!	A-4(7)	A-2-4(0)	A-6(3)		A-2-4(0)	A-6(8)	A-6(2)			A-6(7)	A-6(9)	A-6(10)	A-6(13)	A-6(7)	A-4(2)	A-6(10)	$\Lambda - 7 - 6(17)$	(6)9-V	A-7-6(20)	A-6(9)
Textural	Clay, tr. gravel Peat Clay	Clay, tr. gravel	tr.	tr.	tr.	Peat		tr.		Clay, tr. gravel	Sandy loam w/little	gravel Sandy Clay w/little	gravel		Clay, Little gravel	Sandy clay, tr.	Бтауел	1-69-4(25) 86	Brown Clay	Brown Clay	Brown Clay	Brown Clay	Brown Clay	Br. Sndy. Cl. Lm.	Brown Glay	Brown Clay			Gray Clav
Sample Depth(ft.)	2.0- 3.0 2.0- 4.0 6.0- 8.0	12.0-14.0	0.0- 1.0 2.0- 3.0	2.0- 4.0	2.0- 4.0	4.0- 6.0	0.21-0.01	2.0- 4.0	2.0- 4.0	18.0-20.0	14.5-16.0	0.8- 2.0		-0	-0	-0		Project	2.0- 4.0	8.0-10.0	4.0- 6.0	0.0 - 2.0	3.0- 5.0	13.0-15.0	0.0 - 2.0	2.0- 4.0	9.5-11.5	0.0 - 2.0	10.0-12.0
Offset	37'Rt. E E	E	37'Rt. 37'Rt.	135'Lt.	37'Lt.	37'It.	3/ Lt.	3/'Lt.	17 LL.	/5'Lt.	3/ TE.	37'Lt.		37'Lt.	21'Rt.	15'Rt.			42'Rt.	42'Rt.	42'Lt.	42'Rt.	ن	ت	42'Rt.	42'Lt.	42'Lt.	42'LL.	42'Lt.
Sample	240+00 283+00 283+00	283+00	300+00	354+50	369+00	375+00	37.3400	393+65	20.000	393+65	44T±00	447+00		452+00	469+30	475+35		,	103+00	103+00	108+00	111+00	116+00	1.16+00	129+00	140+00	140+00	152+00	152+00
Job Borehole #	MZ200 MZ108 MZ108	MZ108	MZ215 MZ215	MZ084	MZ033	MZ035	M2040	M2040	MOOLE	M2043	7C07E	MZ054		MZ056	MZ177	MZ160			(high)		(low)	(high)	-	-	(high)	(1.0w)	(low)	-	i I
Map Borehole #	64a 65 65a	65b	66 66a	29	68	69	20	7.7	710	/1a	7/	73		74	75	9/			7.7	77a	78	79	80	80a	81	82	82a	. x	83n
	Job Sample Sample	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL  MZ200 240+00 37'Rt. 2.0- 3.0 Clay, tr. gravel A-6(9) -25- 25 50 29 17  MZ108 283+00 the feat A-4(8) -1- 42 57 47 27  MZ108 283+00 the feat A-4(8) -1- 42 57 47 27	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL  MZ200 240+00 37'Rt. 2.0- 3.0 Clay, tr. gravel A-6(9) - 25 - 25 50 29 17  MZ108 283+00 the feat Clay fr. gravel A-4(8) - 1 - 42 57 47 27  MZ108 283+00 the feat Clay fr. gravel A-4(8) - 24 57 47 27  MZ108 283+00 the feat Clay fr. gravel A-4(8) - 24 57 47 27  MZ108 283+00 the feat Clay fr. gravel A-4(8) - 24 57 49 25 15	Job Sample Sample Sample Sample Sample Sample Station Offset Depth(ft.) Textural AASHTO G S M C LL PL PL MZ200 240+00 37'Rt. 2.0- 3.0 Clay, tr. gravel A-4(8) - 25 - 25 20 26 72 59 MZ108 283+00 E 6.0- 8.0 Clay Tr. gravel A-4(8) - 1- 42 57 47 27 MZ108 283+00 E 12.0-14.0 Clay, tr. gravel A-4(8) - 24- 27 49 25 15 MZ15 300+00 37'Rt. 0.0- 1.0 Clay, tr. gravel A-4(8) - 11- 37 52 29 22 MZ215 300+00 37'Rt. 2.0- 3.0 Clay, tr. gravel A-6(11) - 17- 31 52 29 22 MZ215	Borehole # Station Offset Depth(ft.)   Textural AASHTO G S M C LL PL	Job Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Sample Station Offset Depth(ft.) Textural AASHTO G S M C LL PL PL MZ200 240+00 37'Rt. 2.0- 4.0 Peat	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL  MZ200 240+00 37'Rt. 2.0- 4.0 Peat	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL  MZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(9) -25-22 26 72 59  MZ108 283+00 b 6.0-8.0 Clay tr. gravel A-4(8) -1-42 57 47 27  MZ108 283+00 b 12.0-14.0 Clay, tr. gravel A-4(8) -24-27 49 25 15  MZ215 300+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(11) -17-31 52 36 18  MZ215 300+00 37'Rt. 2.0-4.0 Clay, tr. gravel A-6(11) -17-31 52 36 18  MZ034 354+50 135'Lt. 2.0-4.0 Clay, tr. gravel A-6(8) -26-28 46 26 15  MZ035 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-4(7) -30-21 49 24 15  MZ035 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-4(7) -30-21 37 42 50 39  MZ035 375+00 37'Lt. 10.0-12.0 Clay A-6(10) -4-4 43 53 38 23	# Borehole # Station Offset Depth(ft.)  MZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(9) -25-22 26 72 59 17  MZ108 283+00	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL  MZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(9) -25- 25 50 29 17  MZ108 283+00 b	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL  MZ200 240+00 37'Rt. 2.0- 3.0 Clay, tr. gravel A-6(9) - 25 - 25 50 29 17  MZ108 283+00 b 6.0- 8.0 Clay, tr. gravel A-4(8) - 1 - 42 57 47 27  MZ108 283+00 c 12.0-14.0 Clay, tr. gravel A-4(8) - 24 2 7 49 25 15  MZ215 300+00 37'Rt. 2.0- 3.0 Clay, tr. gravel A-6(11) - 17 - 31 52 29 22  MZ215 300+00 37'Rt. 2.0- 4.0 Clay, tr. gravel A-6(18) - 26 - 28 46 26 15  MZ215 375+00 37'Lt. 2.0- 4.0 Clay, tr. gravel A-6(10) - 4 - 43 53 38 23  MZ035 375+00 37'Lt. 10.0-12.0 Clay  MZ045 393+65 75'Lt. 2.0- 4.0 Clay  MZ046 386+90 37'Lt. 2.0- 4.0 Clay  MZ045 393+65 75'Lt. 2.0- 4.0 Clay  MZ046 386+90 37'Lt. 2.0- 4.0 Clay  MZ047 393+65 75'Lt. 2.0- 4.0 Clay  MZ046 393+65 75'Lt. 2.0- 4.0 Clay  MZ047 - 28 - 21 51 25 16	M2200   Sample   Station   Offset Depth(ft.)   Textural   AASHTO   G   S   M   C   LL   PL     M2200   240+00   37'Rt.   2.0- 4.0   Peat   M2108   283+00   L   C.0- 4.0   Peat   M2108   M2108   283+00   L   C.0- 4.0   Peat   M2108   M2108   M2108   M2109   L   M2108	# Borehole # Startion Offset Depth(ft.) Textural AASHTO G S M C LL PL  MZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C 11 PL MZ200 240+00 37'Rt. 2.0- 4.0 Peat	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL PL MZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(9) -25-25 50 29 17 23+00 b 6.0-8.0 Clay, tr. gravel A-4(8) -1-42 57 47 27 49 25 15 MZ108 283+00 c 12.0-14.0 Clay, tr. gravel A-4(8) -1- 42 57 47 27 A 27 MZ15 300+00 37'Rt. 0.0-1.0 Clay, tr. gravel A-4(8) -11- 37 52 9 22 MZ215 300+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(1) -17- 31 52 36 18 MZ215 300+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(8) -26-28 46 26 15 MZ035 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(8) -26-28 46 26 15 MZ035 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(8) -26-28 46 26 15 MZ035 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(8) -21-37 49 24 15 MZ040 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(8) -21-37 49 24 15 MZ040 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(8) -21-37 49 24 15 MZ045 393+65 75'Lt. 2.0-4.0 Clay, tr. gravel A-6(8) -21-37 49 30 36 81 61 MZ045 393+65 75'Lt. 18.0-20.0 Clay, tr. gravel A-6(8) -21-37 49 30 36 81 61 MZ045 37'Lt. 14.5-16.0 Sandy loam w/little A-24(0) -74- 7 10 NP NP NP MZ056 45+00 37'Lt. 4.0-6.0 Sandy Clay w/little A-24(0) -71- 4 25 16 14 MZ056 45+00 37'Lt. 4.0-6.0 Sandy Clay w/little A-24(0) -71- 4 25 16 14	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL PL MZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(9) -25-22 26 72 57 47 27 MZ108 283+00 b 6.0-8.0 Clay, tr. gravel A-4(8) -1-42 57 47 27 MZ108 283+00 b 12.0-14.0 Clay, tr. gravel A-4(8) -24-27 49 25 15 MZ215 300+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(11) -17-31 52 29 22 MZ215 300+00 37'Rt. 2.0-4.0 Clay, tr. gravel A-6(11) -17-31 52 36 18 MZ215 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(11) -17-31 52 36 18 MZ215 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(10) -4-43 53 38 23 MZ215 393+65 75'Lt. 10.0-12.0 Clay, tr. gravel A-6(10) -4-43 53 38 16 MZ215 393+65 75'Lt. 18.0-20.0 Clay, tr. gravel A-6(10) -4-43 53 38 16 MZ215 393+65 75'Lt. 18.0-20.0 Clay, tr. gravel A-6(10) -24-7 7 10 NP NP MZ215 MZ215 375+00 37'Lt. 14.5-16.0 Sandy loam w/little A-6(3) -52-14 34 26 15 MZ215 MZ215 441+00 37'Lt. 0.8-2.0 Sandy Clay w/little A-6(3) -52-14 34 25 16 14 MZ215 MZ215 45 MZ215 A59 20 21 MZ215 MZ215 A59 20 21 MZ215 MZ215 A59 20 21 MZ215 MZ	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL MZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(9) -25- 22 26 72 59 747 27 MZ108 283+00 b 6.0-8.0 Clay, tr. gravel A-4(8) -1- 42 57 47 27 MZ108 283+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-4(8) -11- 37 52 29 22 MZ200 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(11) -17- 31 52 36 18 MZ015 300+00 37'Rt. 2.0-4.0 Clay, tr. gravel A-6(11) -17- 31 52 36 18 MZ015 305+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(11) -17- 31 52 36 18 MZ015 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(11) -17- 31 52 36 18 MZ015 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(11) -17- 31 52 38 23 MZ015 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(10) -4- 43 53 38 16 MZ015 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(10) -4- 43 53 38 16 MZ015 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(10) -4- 43 53 38 16 MZ015 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(10) -4- 43 53 38 16 MZ015 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(10) -4- 43 53 38 16 MZ015 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(10) -7- 19 54 28 16 MZ015 37'Lt. 18.0-20.0 Clay, tr. gravel A-6(10) -7- 28- 21 4 34 26 15 MZ015 37'Lt. 14.5-16.0 Sandy Ioam W/little A-2-4(0) -7- 28- 21 4 34 26 15 MZ015 45 MZ015 37'Lt. 4.0-6.0 Sandy Clay W/little gravel A-6(10) -7- 4- 4 31 31 13 13 13 13 13 13 13 13 13 13 13	Machole # Station Offset Depth(ft.)   Textural AASHTO G S M C II. PL	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL WZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel	M2206   Sample   Sample   Sample   Sample   Sample   Sample   Sample   Barchole # Station   Offset   Depth(ft.)   Textural   AASHTO   G   S   M   G   LL   PL	# Borehole # Sample   Sample	# Borehole # Sample  Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL  MZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(9) -25-25 50 29 17  MZ108 283+00 b. 6.0-8.0 Peat A-4(8) -27-22 26 72 59  MZ108 283+00 b. 12.0-14.0 Clay, tr. gravel A-4(8) -1-42 57 47 27  MZ215 300+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(11) -17-31 52 29 25 15  MZ215 300+00 37'Rt. 2.0-4.0 Clay, tr. gravel A-6(11) -17-31 52 29 22 15  MZ033 354+50 135'Lt. 2.0-4.0 Clay, tr. gravel A-6(11) -17-31 52 29 22 15  MZ035 375+00 37'Lt. 2.0-4.0 Clay, tr. gravel A-6(11) -17-31 52 29 22 15  MZ036 386+40 37'Lt. 2.0-4.0 Peat A-6(11) -4-4 35 38 38 23  MZ045 393+65 75'Lt. 10.0-12.0 Clay  MZ045 393+65 75'Lt. 18.0-20.0 Clay, tr. gravel A-6(8) -26-38 46 26 15  MZ045 393+65 75'Lt. 2.0-4.0 Peat A-6(10) -4-4 33 33 38 23  MZ045 393+65 75'Lt. 14.5-16.0 Sandy loam W/little A-2(0) -74-7 10 NP NP  MZ054 447+00 37'Lt. 0.8-2.0 Sandy Clay w/little A-6(3) -52-14 34 26 15  MZ055 452+00 37'Lt. 4.0-6.0 Sandy Clay w/little A-6(3) -52-14 34 26 15  MZ056 452+00 37'Lt. 2.0-4.0 Clay, Little gravel A-6(3) -52-16 38 31 16  MZ056 452+00 37'Lt. 0.8-2.0 Sandy Clay w/little A-6(3) -52-16 38 31 13  MZ056 452+00 37'Lt. 4.0-6.0 Sandy Clay w/little A-6(3) -52-16 38 31 13  MZ056 452+00 37'Lt. 2.0-4.0 Clay, Little gravel A-6(8) -74-7 10 NP NP  MZ056 452+00 37'Lt. 4.0-6.0 Sandy Clay w/little A-6(3) -52-16 38 31 13  MZ056 452+00 47'Rt. 2.0-4.0 Brown Clay A-6(12) 44 25 16 14  MZ167 465+30 21'Rt. 2.0-4.0 Brown Clay A-6(12) 42 25 18 (high) 103+00 42'Rt. 80-010.0 Brown Clay A-6(12) 23 13 14 34 32 18 (high) 103+00 42'Rt. 80-010.0 Brown Clay A-6(12) 23 13 14 34 32 18	# Borehole # Station Offset Depth(ft.) Textural AASHTO G S M C LL PL MIZ200 240+00 37'Rt. 2.0-3.0 Clay, tr. gravel A-6(9) -25 - 25 26 72 59 17	# Borehole # Sample   Sample	# Borechole # Sample   Sample	# Borehold   Sample	Miles   Sample   Sa	# Borehole # Stanple   Sample   Sattion (ffset Depth(fft.)   Textural   AASHTO   C S   N   C   L  PL   PL   MZ108   283+00   L   2.0-4.0   Clay   Cl	# Job NZ108



PART I - Continued

PL PI	26 28 23 25 27 32 17 16		19 32 23 28 19 17 22 23 15 11	20 26 20 34 20 34 21 14 21 32 22 16 21 22 16 22 16 21 21 16 12 26 32 20 22	25 15 20 22 16 11 17 11
LL F	54 2 48 2 59 2			7446 446 445 445 445 445 445 445 445 445	40 42 27 1 28 1 40
Percent G S M C	9 43 48 11 41 48 13 41 46 26 36 38	31 52 62 42 48		10 25 65 17 39 44 10 42 48 23 35 42 11 39 50 9 46 45 47 25 28 14 32 54 40 33 27 19 37 44 13 49 38 22 33 45	1 28 39 32 0 27 34 39 7 30 31 32 0 32 31 47
ASHTO	A-7-6(18) A-7-6(16) A-7-6(20) A-6(11)	A-6(11) A-4(0) A-7-5(17) A-4(8) A-7-6(19) A-7 6(15)	A-7-6(18) A-7-6(17) A-6(10) A-7-6(14) A-6(6)	A-7-6(15) A-7-6(13) A-7-6(19) A-6(10) A-6(10) A-7-6(18) A-7-6(18) A-6(6) A-7-6(13) A-6(9) A-7-6(13) A-7-6(13)	A-7-6(10) A-7-6(13) A-6(6) A-6(8) A-6(12)
Classification Textural A	Black Clay Brown Clay Brown Clay Brown Clay	O S I		Gray Clay Brown Clay Brown Clay Brown Clay Black Clay Brown Clay Brown Clay Brown Clay Brown Clay Brown Clay Brown Clay Brown Clay Brown Clay Brown Clay Brown Clay	No. 63 (4) S.R. 114 Clay Clay Clay Clay Clay Clay
Sample et Depth(ft)	Lt. 0.0-2.0 Ft. 2.0-4.0 Rt. 1.0-3.0 Rt. 5.0-7.0	11.0-13 13.0-15 1.0- 3 3.0- 5 0.0- 2		Rt. 15.0-11.0 Rt. 15.0-17.0 Rt. 0.0- 2.0 Rt. 4.0- 6.0 Lt. 0.0- 2.0 Lt. 2.0- 4.0 Rt. 1.0- 3.0 Rt. 5.0- 7.0 Rt. 9.0-11.0 Rt. 9.0-11.0 Lt. 0.0- 2.0 Lt. 4.0- 6.0	S-Project N Lt. 0.0- 0.7 Lt. 0.7- 3.0 Lt. 3.0- 4.5 Rt. 0.8- 4.5 Lt. 1.1- 6.0
0ffs				4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	161 161 179 178 178
Sample Station	164+00 179+00 185+00 185+00	185+00 185+00 200+00 200+00 203+00 215+00	215+00 230+00 230+00 245+00 245+00	245+00 245+00 251+00 263+00 278+00 278+00 278+00 287+00 287+00 302+00 302+00	10+00 10+00 10+00 148+00 158+00
Job Borehole #	-(10w)- 	 -(10w)- -(10w)- -S.W. Lac	 (high)	- (10w)- - (10w)- - (10w)- - (10w)- 	
Sorehole #	84 85 86 86a	86b 86c 87 87a 88	89a 90 90a 91	91a 91c 92 93 94 94 95 95 956 96	97 97a 97b 98



PART I - Continued

	PI	28 12 14	36 NP	22 8			NP 10.8	•			15.0 pcf)	NF 13.6	NP 3 O	10.4	
							C				17.3 15.0 132.0(pcf)	8	NP 1.2 3	5.3	
	PL	42 21 28 28	26 NP	21 20			00				.3 1 13	6.	C	5.7 1	1011
	LL	70 33 42	62 NP	43		%					8 32 dens	.0 32	10.7 NP	13.3 25	) nd i t
	O	33 26 28	30	40 22 5		202 =	6	1		,	43.1 27.8 32.3 ax. wet dens			5 13	an C
Percent	×	37 45 36	7,0	45 29 18.		RQD		33%			43. nax.	4 – 13.   36.1		66.5	30%; artesian condition
Per	S	30 29 25	30	15 47	ver	70% @ 2.5;	5.244.0	40.T		iver	3.8 25.3 (pcf); ma	29.4	45.1	5.7 20.5	ធ គ
	ß	0 0 11	0 9	onte	sh Ri		5.2	U.0 ); R(		ie Ri	3.8 7(pc	57	15.1	5.7	30%
Classification	AASHTO		.s. 24 A-7-6(25)	A-4(0) A-7-6(20) 0 15 A-4(1) 2 47 Opt. Moisture content	224 over L. Wabash River	@ 2.0'; RQD =	A-4(0)	A-6(4) olomite @ 18.0	1.9'; RQD=30%	over Salamonie River	A-6(9) 3.8 25.3 43.1 27.8 32.3 17.3 15.0 dry dens114.7(pcf); max. wet dens132.0(pcf)	A-1-a(0) A-6(6)		A-4(U) A-4(5)	bedrock w/RQD =
Classif	Textural	Peat Marly Peat Marly Peat	n PI	Sandy Loam Clay Clay Loam - 106.3(pcf); Op	- 1(1), S.R. 224	Silt and sand to dolomite @ 2.0'; RQD = 70%	Loam	13.5-15.0 Loam A-6(4) 0.0 40.1 hard massive, fractured dolomite @ $18.0$ ; RQD =	soft to dolomite @	3055(1), S.R. 218	Clay loam 14.9; max.		Sandy Loam		lmst./dolom. be
	Sample Depth(ft.)	0.0- 1.4 1.4- 6.8 2.6- 6.8	ject 4.5	3.0- 4.5 1.5- 2.0 4.5- 6.0 Dry Density	ect No. 158 -	Silt and s	6.0- 7.5		Gray, soft	RS-Project No. 30	2.5- 4.0 Opt. moist	13.5-15.0	15.0-16.0	25.0-26.5	sal @ 37.5';
	Offset	25'Lt. 25'Lt. 13'Lt.	37'Rt.	52'Lt. 52'Lt. E Max.	F-Proje	33'Lt.	30.3 Kt. 13'Lt.	13'Lt.	33'Rt.	RS-P1	'n	30 O'1.F.	30.0'Lt.	30.0'Lt. 30.0'Lt.	Auger refusal
	Sample Station	309+00 309+00 379+00	3+25	27+50 27+50 61+00		11+03.5	12+87	12+87	13+70		552+00	552+00	553+15	553+15	
	Job Borehole #		RB-1	RB-6 RB-6 RB-8		TB-1	TB-2 TB-3	TB-3	TB-4		RB-1.CBR	RB-1	TB-1	TB-1 TB-1	
	Map Borehole #	100 100a 101	102	103 103a 104		105	106 107	107a	108		109	109a	110a	110b 110c	

# PART I - Continued

PI	2.1	SN SN	11.0 6.9	L <sub>I</sub>			4 -		11													ر. در	)
	7			3		19	NP	NP NP		30	47	19	12	10	10	14	11		217	N		6 9	3
PL	12.	NP	16.6 19.7	TRI .		14	NP	L3 NP		31	29	26	23	16	21	21	18		N.I.	N a		15.3	
LL	14.8	NP	27.6 26.6	.78%		34	NP	C7 NP		70	9/	45	35	26	48	35	29		E.	NP		24.8	
O	6.4	9	22.2	v/RQD=78%		29		T !		7.7						29			3 6	0.		19.4	
nt M	27.9	2.	41.7	. n		42	0	4, 12		9	9+	55	99	34	10.	54	36		0	41.9		54.4	
Percent Ș M	42.8	2.9		)			96			7	7	-,	<b>u</b> ,	. ,	.,	1 5			c	.5		22.7	
G	22.9 4	44.5 52.9	3.4 3 50.1 3 76 8 5	ove			0 0	7 7	Etna	- 7-		- 2-	-15-	-28-	-13-	-117-	-27-	ek		36.5 56		3.5 2	
		0) <sup>7</sup>	66	<b>a</b> 1	Creek	$\overline{}$		0) 2	of Mt.	(77	55)							r Creek			-2		751
ion AASHTO	A-2-4(0)	A-1-6(0)	A-6(4) A-2-4(0) A-1-6(0)	ered	Pony	A-6(11	A-3(0)	A-1-6(0)	North o	A-7-5(44)	)9-/-	A-7-6(22)	A-6(10)	A-4(5)	A-7-6(25)	A-7-0(2 A-6(11)	A-6(6)	Silver	(0) 7 6 4	A = 2 - 4 (0) A = 1 - b (b)	w/RQD of 15	A-4(5) A-6(16)	w/RQD of
Classification 1	₽	A lomit	4; 4	weathered	over	A	∢ <	4 ≪	oN 6	A	A			A	Ϋ́ «		A	over	<	₹ ₹	w/RQ	< <	3
assif		avel Sand ': do	vel	vel of	105			Sand	37 e				, loam		_	, loam		105		and	tone		Limestone
Cl ral	Loa	e gr 11y 17.8	loam Gravel		S.R.	Loam			SR.			Clay	clay	;	Clay	Clay	•	S.R.	1001	1y S	Imes	loam	I, Ime
C Textural	Sandy Loam	W/some gravel 10.0-11.5 Gravelly Sand A-1-6(0) 4 Auger refusal @ 17.8': dolomite bedrock	Clay loam Sandy Grav Sandy Loam	w/some 2.5';			Sand	Gravelly	P.E.,	Clay	clay	Silty	Silty	Clay	Silty	Silty	Clay		Candy loam	Gravelly Sand	13.0; Limestone	Silty	5.21;
(t)	5.5	5 efus	~ O ~		3335(2)				(12)						0.7		1	3335(1)	٠	0.			_
Sample Depth(ft)	5.0- 6	.0-11.5 ger ref	6.0- 7.5 13.5-15.0 28.5-29.5	Refusal	No.	.5- 5	38.5-25.0	5-10	101 (						T.O- 2		-	No.	c	3.5- 5	Refusal	3.5-15.0	Refusal
					lect		38							7 ,	-i <	0	7.	ject			Ref		Ref
Offset	30'Rt.	30'Rt.	25'Rt. 25'Rt. 25'Rt.		RS-Project	11 Rt.	30'Rt.	11 'Lt.	F-Project	37'Rt.	37'Rt.	37'Rt.	37'Rt.	3/ KC.	37 Rt.	37'Rt.	7 Rt.	ST-Project	11.4	22'Lt.		18'Rt.	
0	5 3		222		XI	<del>-</del>	ين بي	) <del>-</del> -i		'n	33	m i	m i	'nċ	א ה	, m	37	S	2	22	,	2 2	
Sample Station	554+18.5	554+18.5	555+91 555+91 555+91			50+36	49+87	49+64		9	9	9 9	9 5	777	2 9	F25	+25		٥.	-03	c	-23	
Sam	554	554	555 555 555			50	4 4 9 9	49		958+00	958+00	958+00	00+196	7004	1037+00	1101+25	1101+25		100+03	100+03	,	100+23	
1e #																							
Job borehole	TB-2	TB-2	TB-3 TB-3 TB-3			TB-3	1.B-2 TB-2	TB-1		2	2	5	9 1	, ¿	24	40	40		T.B-3	TB-3	i i	TB-4	
J.																							
Map borehole	Т.	1115	112 112a 112b			5	114 114a	3		9	6a	6b ,	<b>~</b> ~	0 0	9a	0	0a			La		2.1	
Map	111	11	112 112 112			115	11	113		116	116a	1165	118	110	119a	120	120a		121	121.a	100	122a	



APPENDIX B Part II

# Miscellaneous Information

Notes	Limestone encountered @ 1.0 - 7.0 ft.; overburden generally composed of sandy loam (A-4) surface soil and silty clay-loam (A-6) subsoil. Parent materials are thin outwash or recent alluvium over residual limestone soil or limestone bedrock. Elevation of bedrock approximately 688' a.m.s.l.	Sounding show depth of peat or muck in small bogs north of Huntington as much as 22.0 ft. General profile consists of: a) 0'-3' of clay with trace gravel; b) 3'-6' organic soil; c) 6'-14' of muck, and d) clay with trace gravel beneath 14.0'.	Ground moraine soil types using the AASHTO classification system shared the following distribution along the S.R. 37 Bypass north of Huntington:	Soil Type Percent	9	A-4 40 A-6 40 A-7-6 6 (peat)	Limestone encountered at depth of 13.0 to 20.0 feet. General profile consists of a sandy loam (A-2-4) surface soil which is underlain at about 3 feet by alluvial sands and gravels (A-1-6) to a depth of about 5 to 13 feet. Silty loam (A-4) or silty clay (A-6) - till overlies limestone bedrock.
Soil Survey Project	F-Project 888(3), S.R. 37 over Wabash River.	F-Project 888 (1), S.R. 37 Bypass north of Huntington.					F-Project 3335 (1), S.R. 105 over Silver Greek.



Part II, Continued

Notes	Limestone encountered as shallow as 3 feet and up to 23 feet deep. General soil profile consists of 1.0 feet of a sandy loam surface soil which is underlain by silty loam or silty clay-loam to limestone bedrock.	Limestone encountered at depths of from 7.0 to 25.0 feet. General soil profile consists of 1.0 to 3.5 feet of a sandy loam surface soil which is underlain by silty loam or sandy loam alluvial material. The surface or subsoil is underlain by weathered, residual limestone which lies on the limestone bedrock.	General soil profile consists of 1.0 to 3.0 feet of a fine sand, silt loam, or sandy loam surface soil which is underlain by alluvial sand and gravel and sandy loam parent materials. Silty loam or silty clayloam till underlies the alluvial material.	Limestone encountered at 12.5 to 15.5 feet of depth with RQD of 0%-15%. General soil profile consists of 0.3 feet of a silty loam surface soil which is underlain by a sandy clay, silty clay, or silty loam subsoil to 7.0. Silty clay-loam or silty clay-till overlies limestone bedrock.	
Soil Survey Project	Structure No. 221-35-6042, S.R. 221 over Wabash River.	Structure No. 221-D-5451, S.R. 221 over Salamonie River	F-Project 101 (8), S.R. 9 over Salamonie River.	ST-Project No. 3635 (B), S.R. 124 over Brook Greek	



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